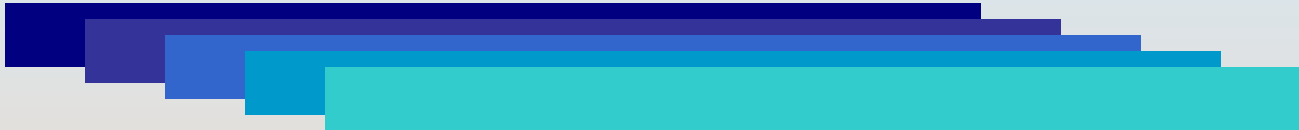


NCHRP 9-59 Update



May 10, 2018
FHWA ETG
Fall River, MA



Advanced Asphalt Technologies, LLC



"Engineering Services for the Asphalt Industry"

Outline

- Introduction
- Materials
- Binder rheology
- Strain capacity, failure envelope
- Mixture vs binder performance
- Delta Tc, GRP, DENT, extended BBR
- Summary, conclusions

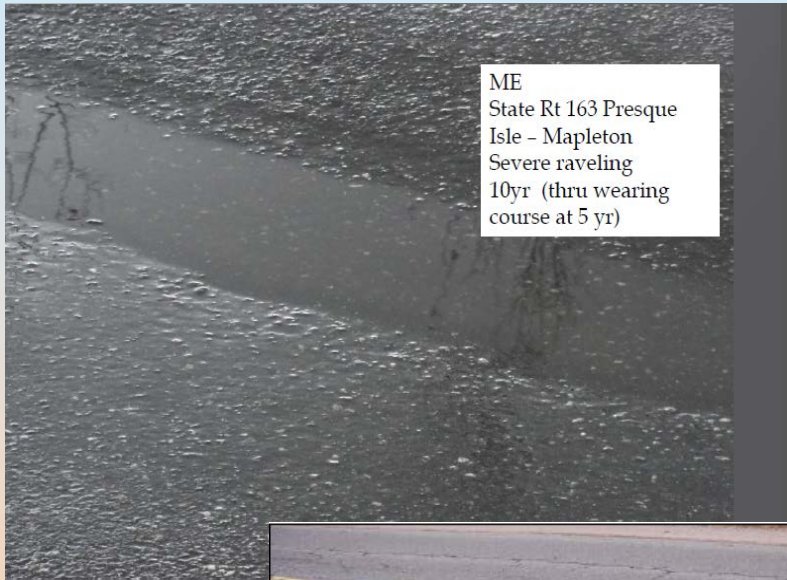


NCHRP 9-59 Objective

The primary objective of NCHRP 9-59 is to develop a test or tests that will help to effectively and efficiently control the properties of asphalt binders that contribute to the fatigue resistance of asphalt mixtures



Problem



Hwy 41 North of Kaladar (1999)



Hesp et al., *Proceedings CTAA*, 2009

*Bill Ahearn,
Pamela Marks,
Simon Hesp*



What is causing these failures?

- Problem binders
 - Excessive brittleness
 - Poor healing
 - Misleading BBR grading
- Delta Tc, R-value, GRP and DENT are all indicators of the same problem



Over last month...

- Further progress made in data analysis since TAI meeting in Savannah
- Slight change in assumed failure envelope significantly improved results
- May be a few more changes as final report is compiled and reviewed...



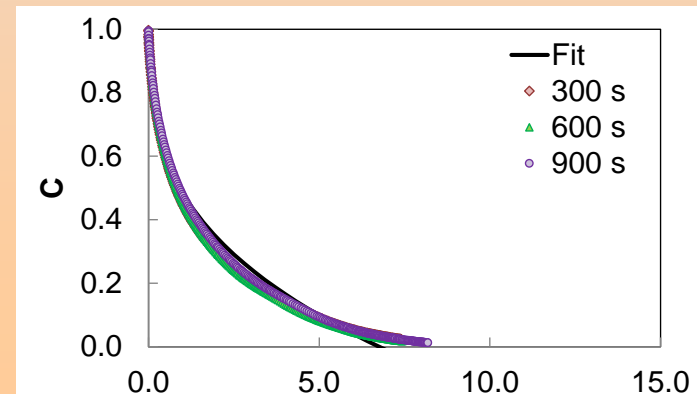
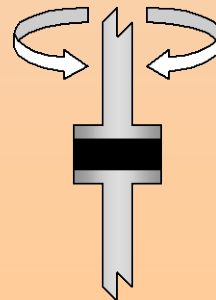
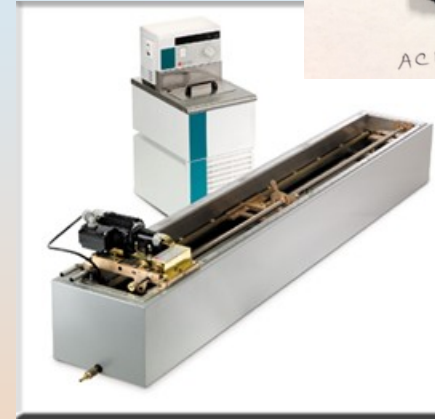
Binders included in NCHRP 9-59

- NCHRP 9-59, 8 polymer modified, 8 non-polymer modified
- 2 REOB, 2 oxidized, 1 PPA
- RTFOT + 40 hour PAV
- SHRP binders, RTFOT aging
- ALF, MNRoad, Westrack binder, miscellaneous aging



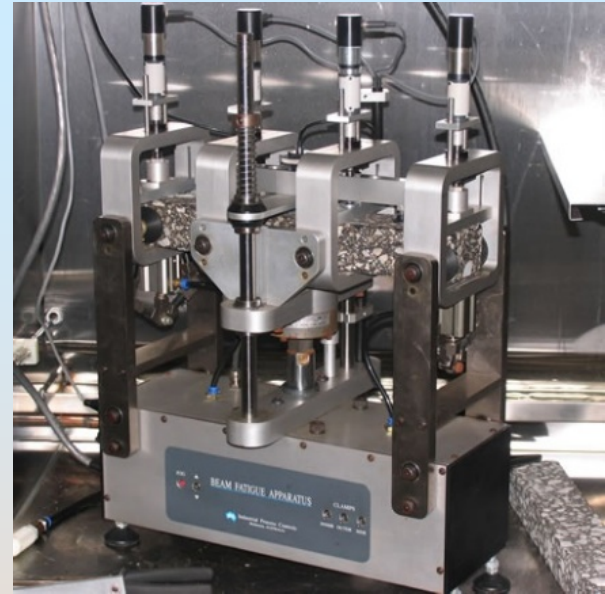
Binder Tests

- DSR / master curve
- DSR / linear amplitude sweep (LAS)
- Double-edge notched tension (DENT)
- Various tests from previous research

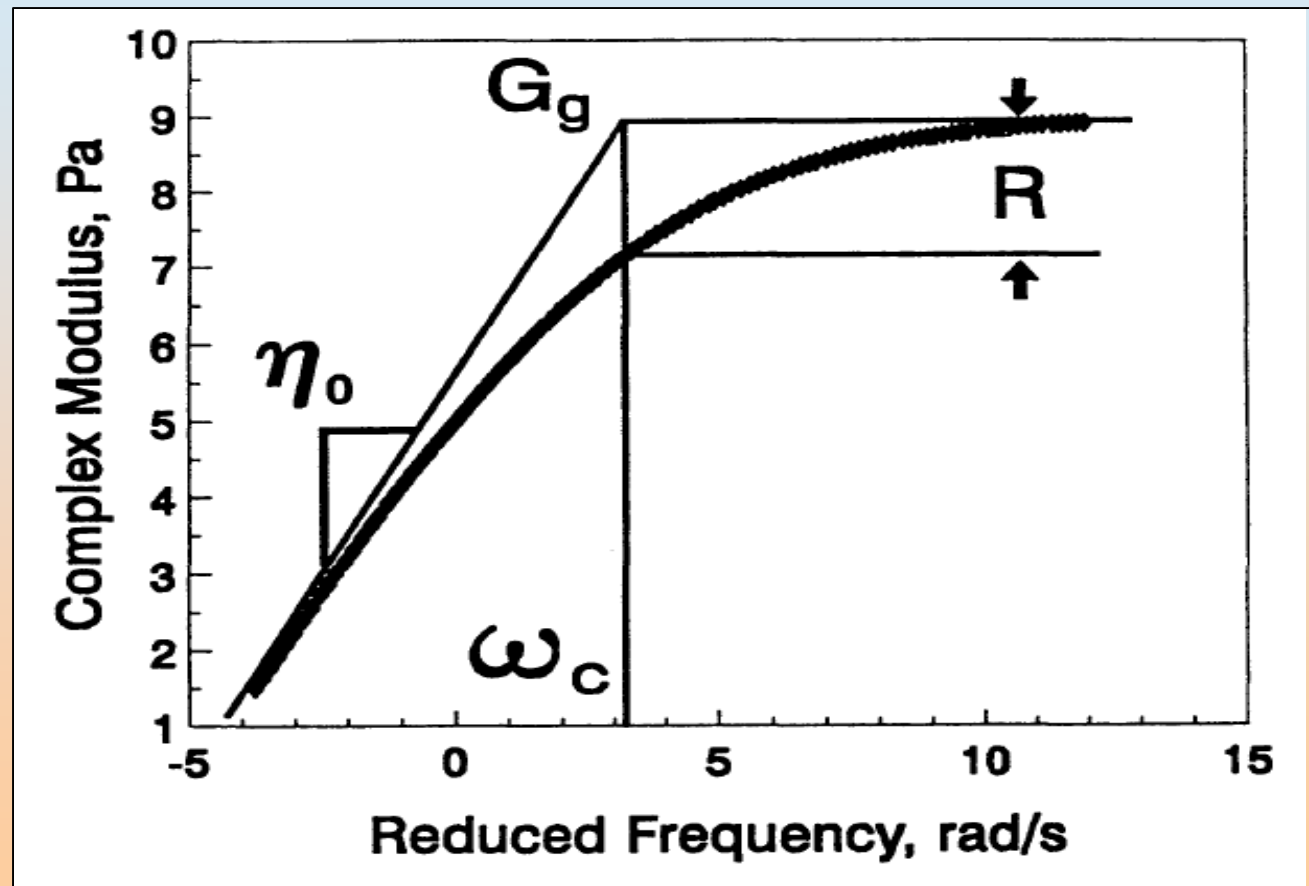


Mixture tests

- Flexural fatigue
- Uniaxial fatigue
- Healing
- Loose mix aging, 95 C for 5 days
- Various tests from previous research



Binder rheologic type and R value



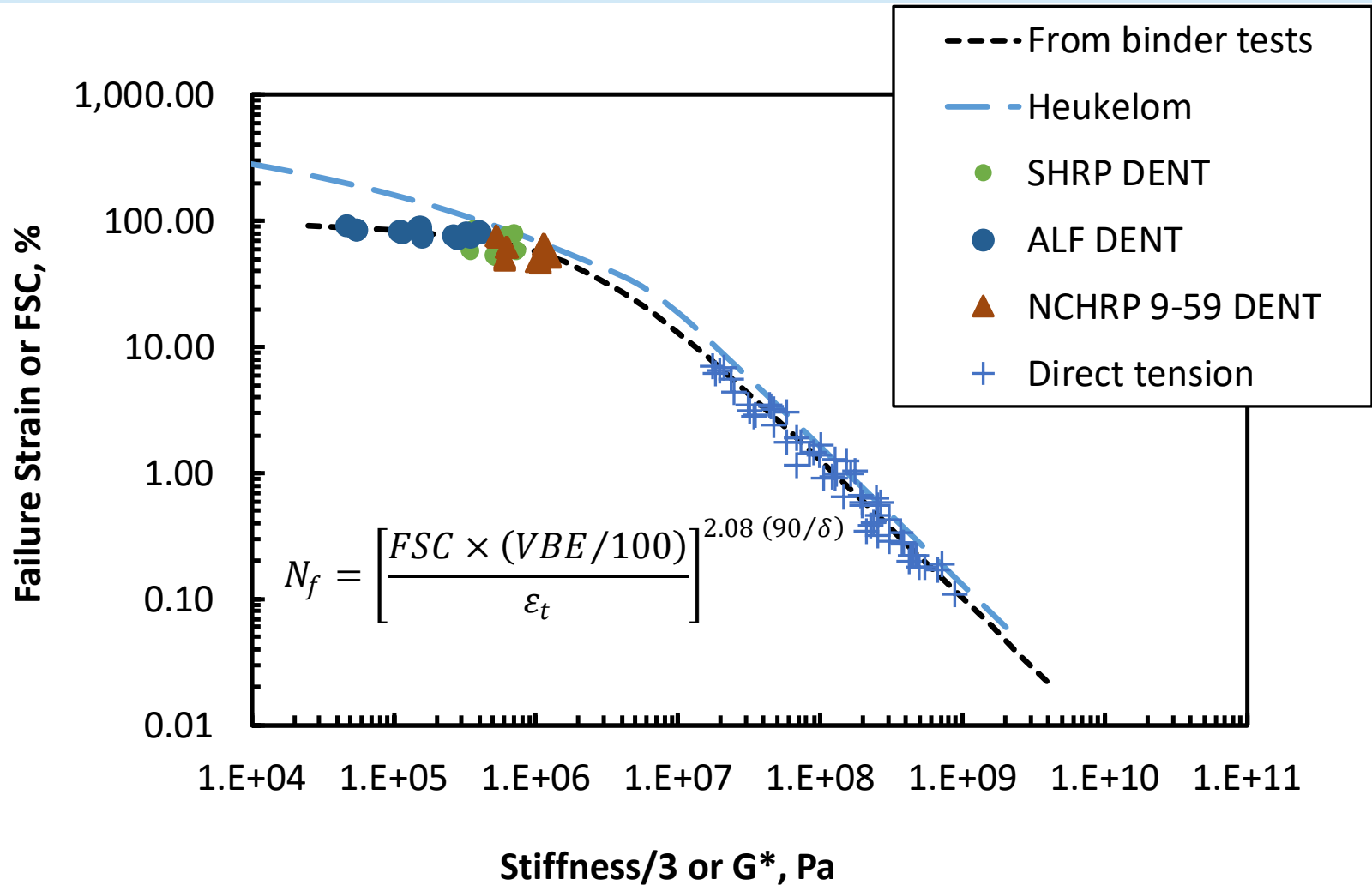
Some notes on R-value

- Polymer modified binders and heavily aged non-modified binders are rheologically complex
- R can be calculated from a DSR point measurement as long as $|G^*|$ is about 10 MPa or higher:

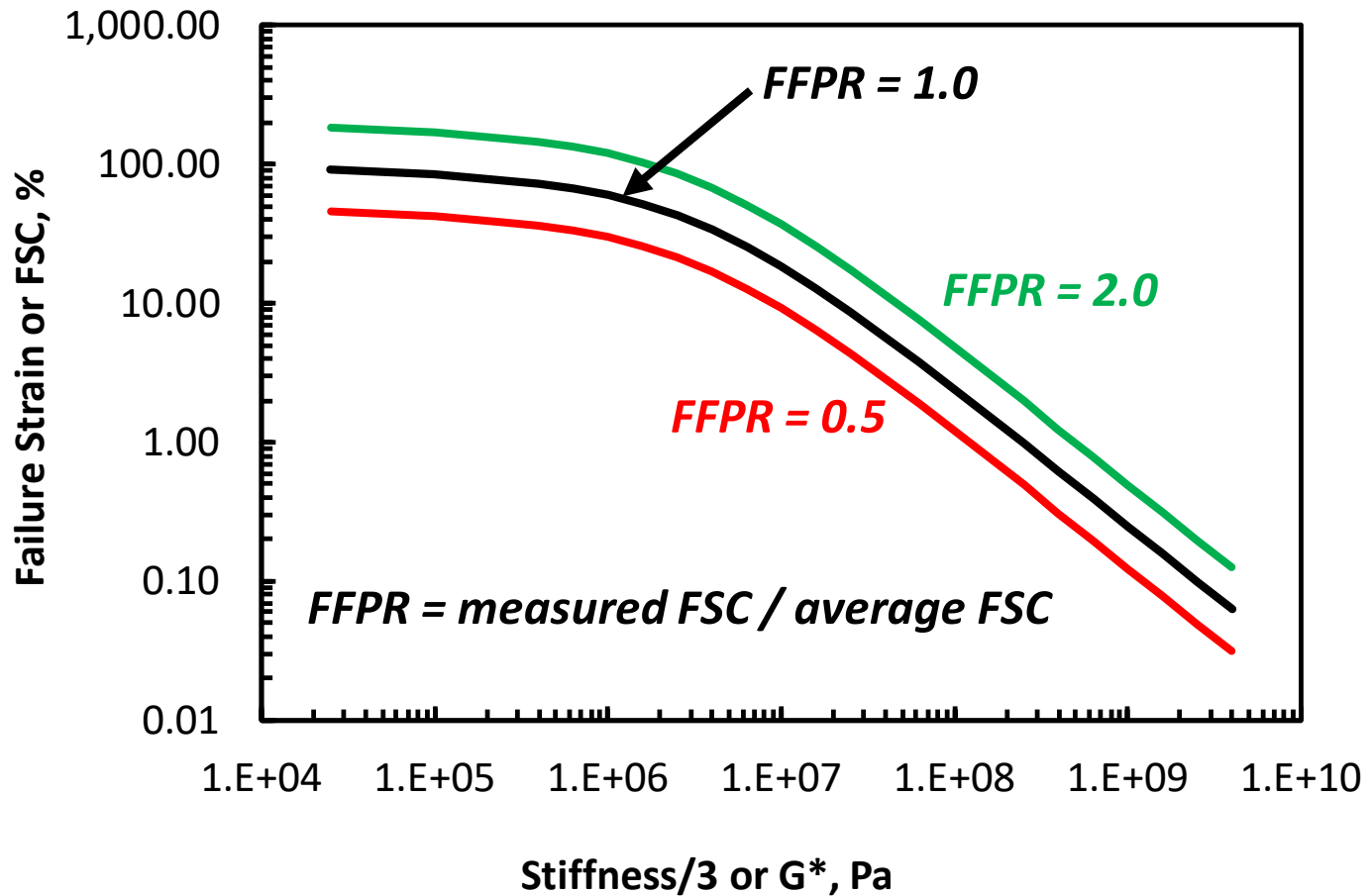
$$R = \log(2) \frac{\log(|G^*|/1 \times 10^9)}{\log(1 - \delta/90)}$$



Asphalt Binder Failure Envelope



Fatigue/fracture performance ratio FFPR



More on FFPR

- FFPR is an indicator of inherent fracture and fatigue resistance
- FFPR $\gg 1$ indicate good fatigue performance, FFPR $\ll 1$ indicate poor performance
- For the binder studied in NCHRP 9-59, FFPR values ranged from about 0.4 to 2.



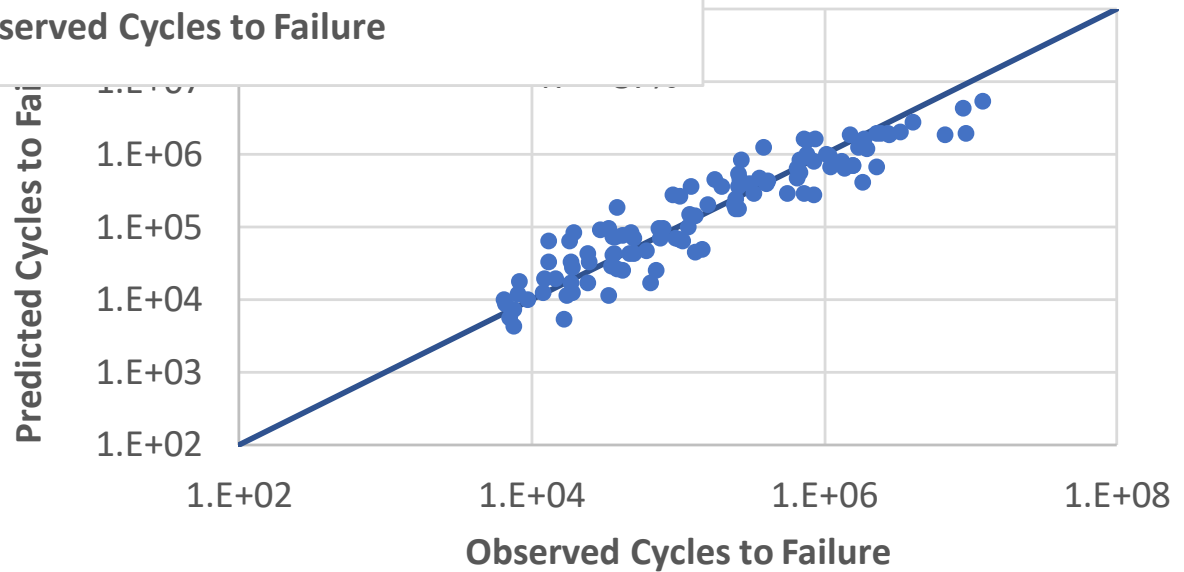
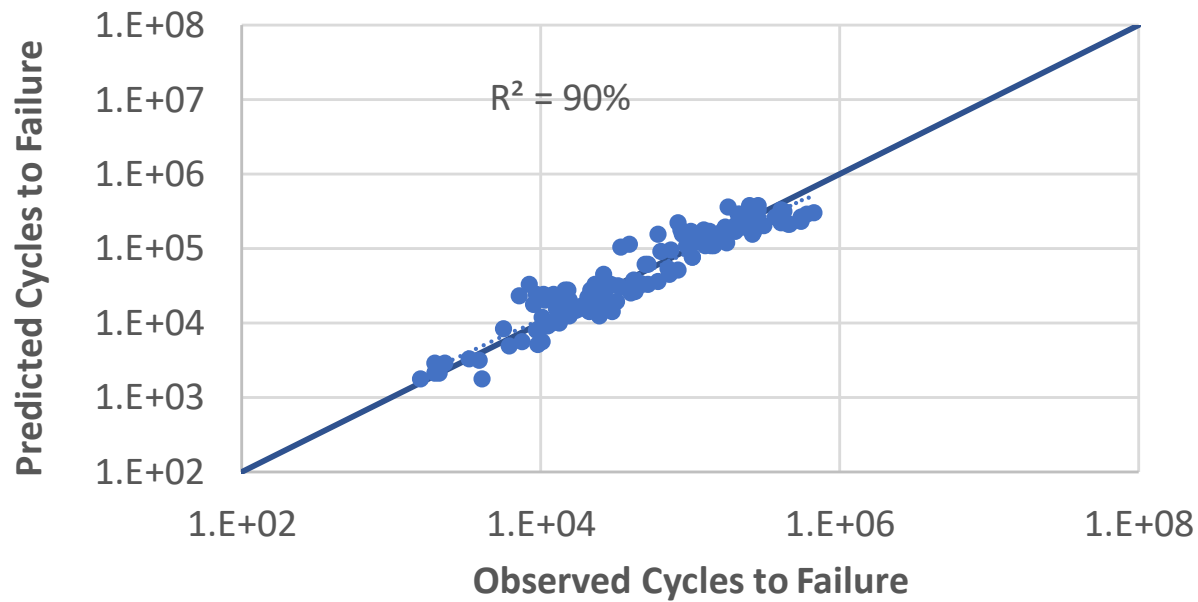
GFTAB model

$$N_f^{\wedge} = \left[\frac{FFPR_i \times FSC^* \times (VBE/100)}{\varepsilon_t} \right]^{k_1(90/\delta)}$$

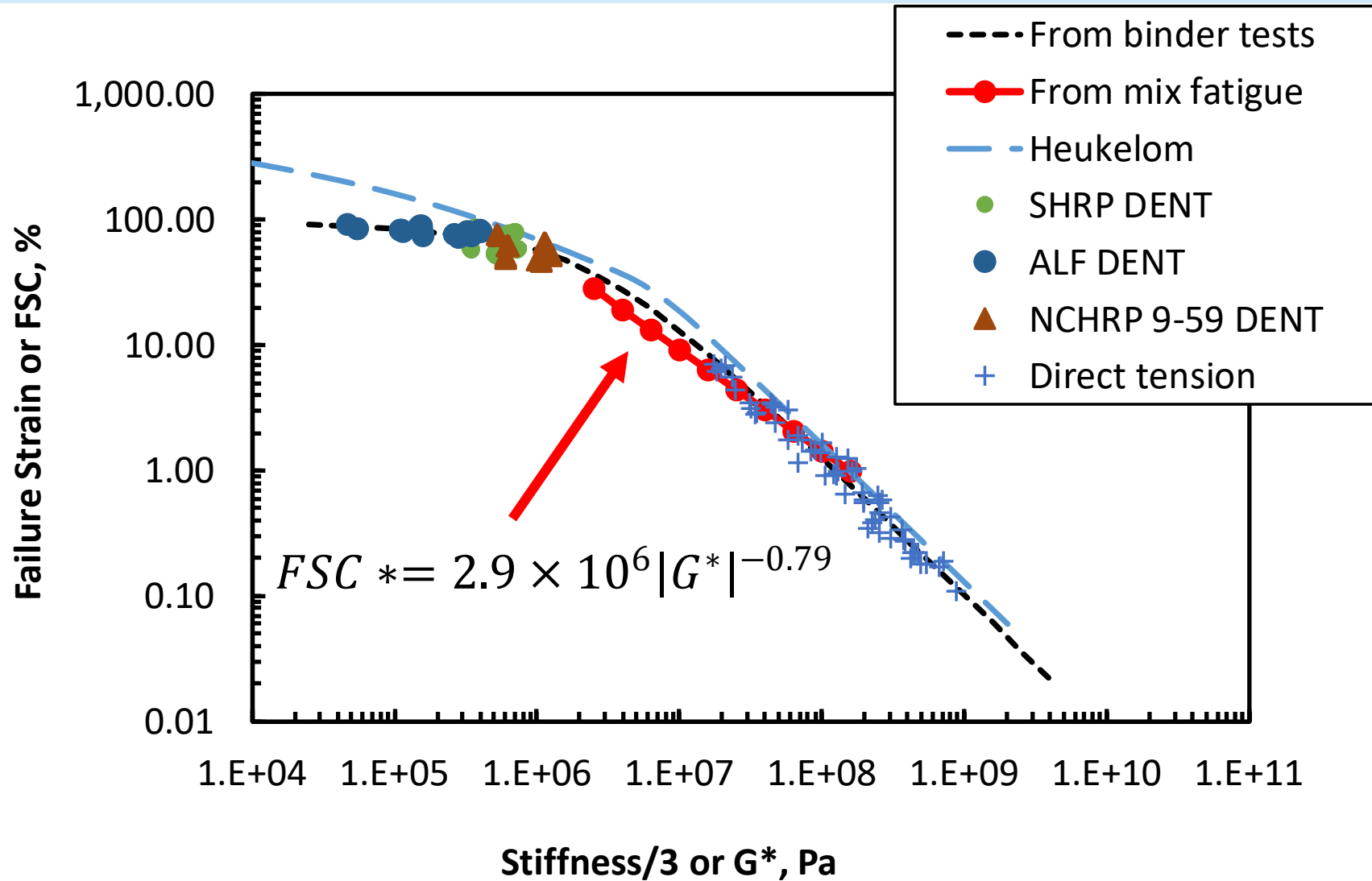
FFPR represents the overall strain tolerance of each binder. FSC is the typical failure strain at any given $|G^|$. K_1 was found to be 2.08.*



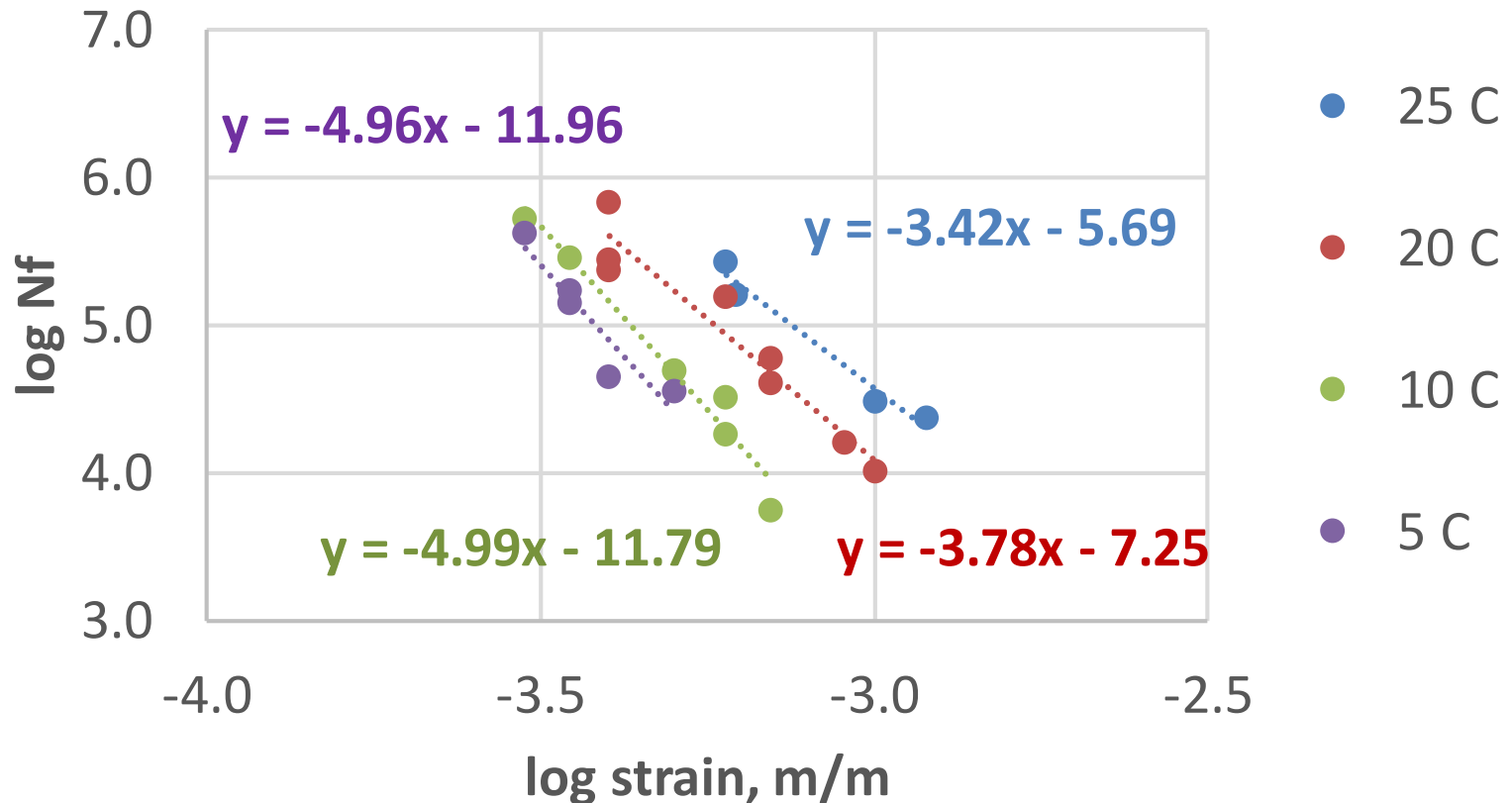
Results of GFTAB model



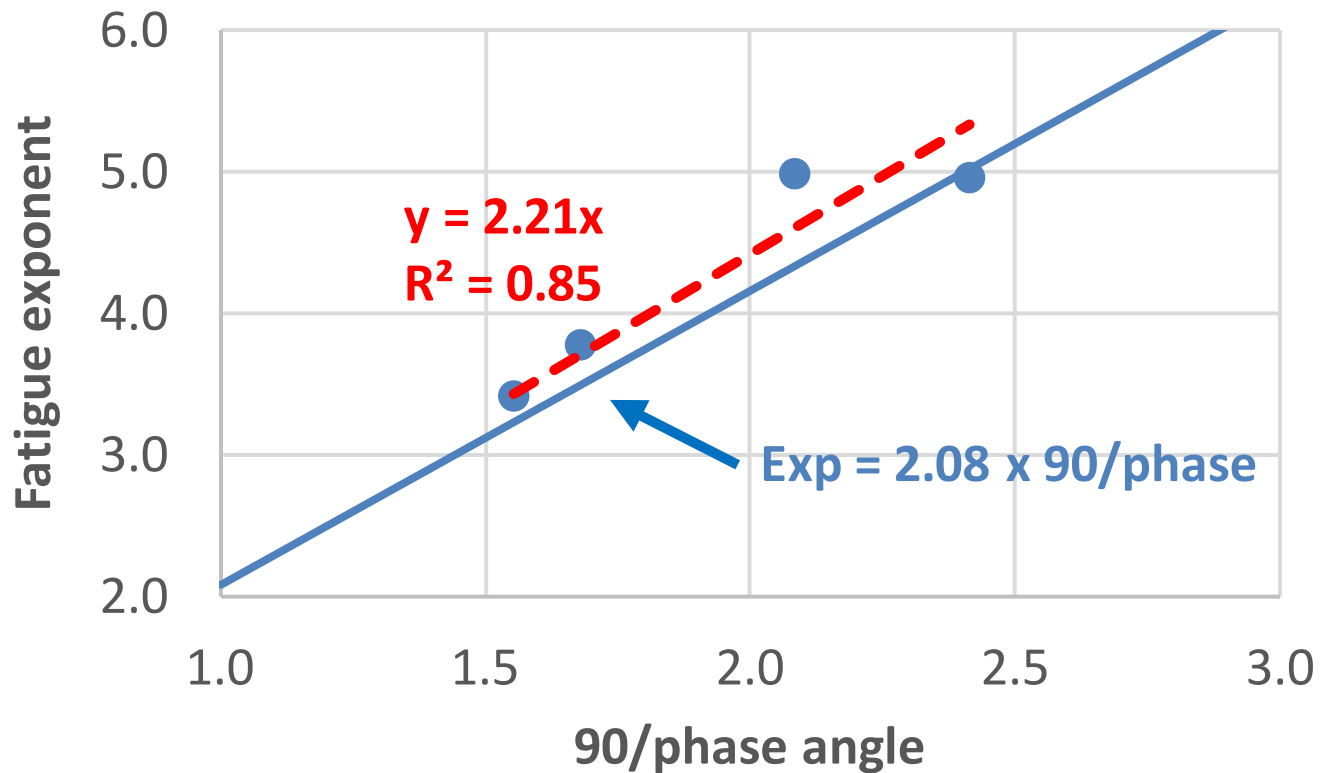
Is GFTAB for real?



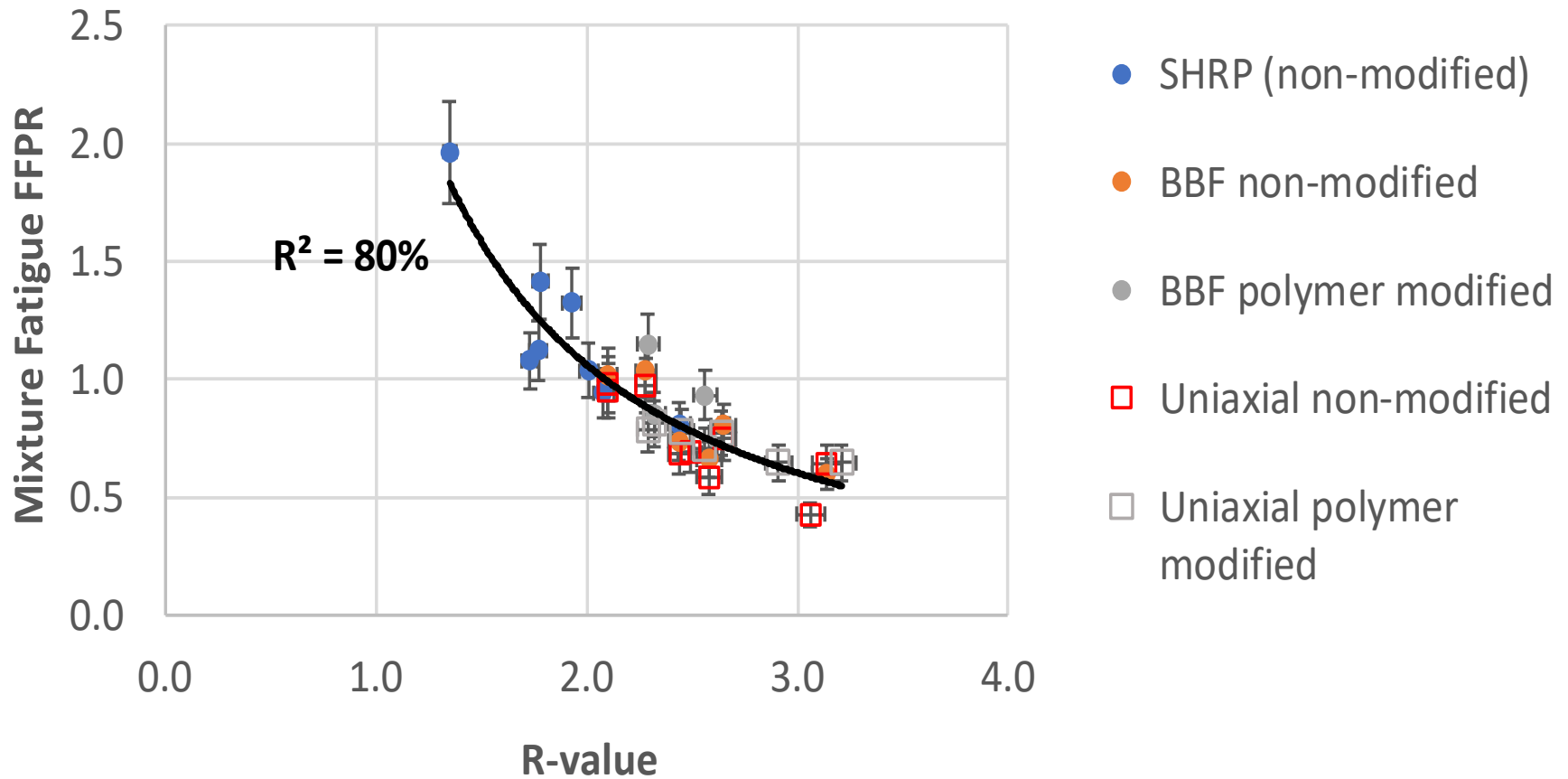
SHRP AAD-1: Fatigue exponents at different temps



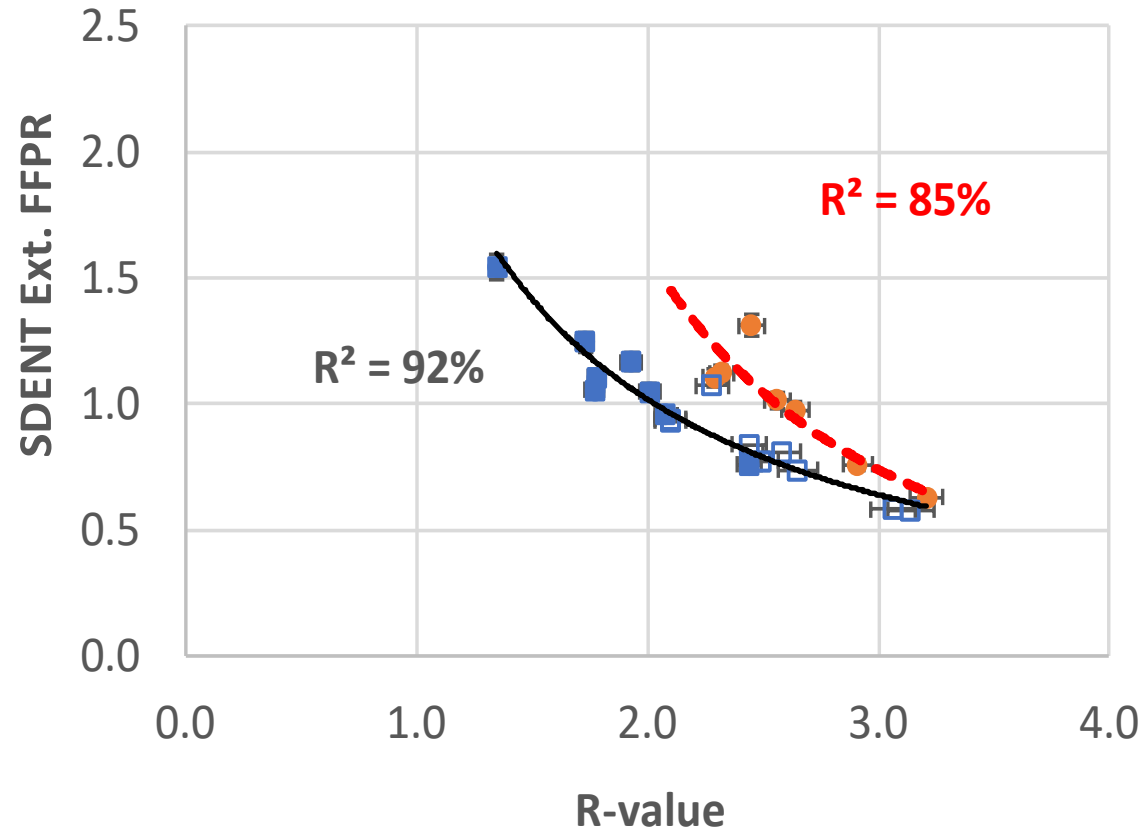
SHRP AAD-1: Fatigue exponent vs. phase angle



Mixture Fatigue FFPR and Binder R-value



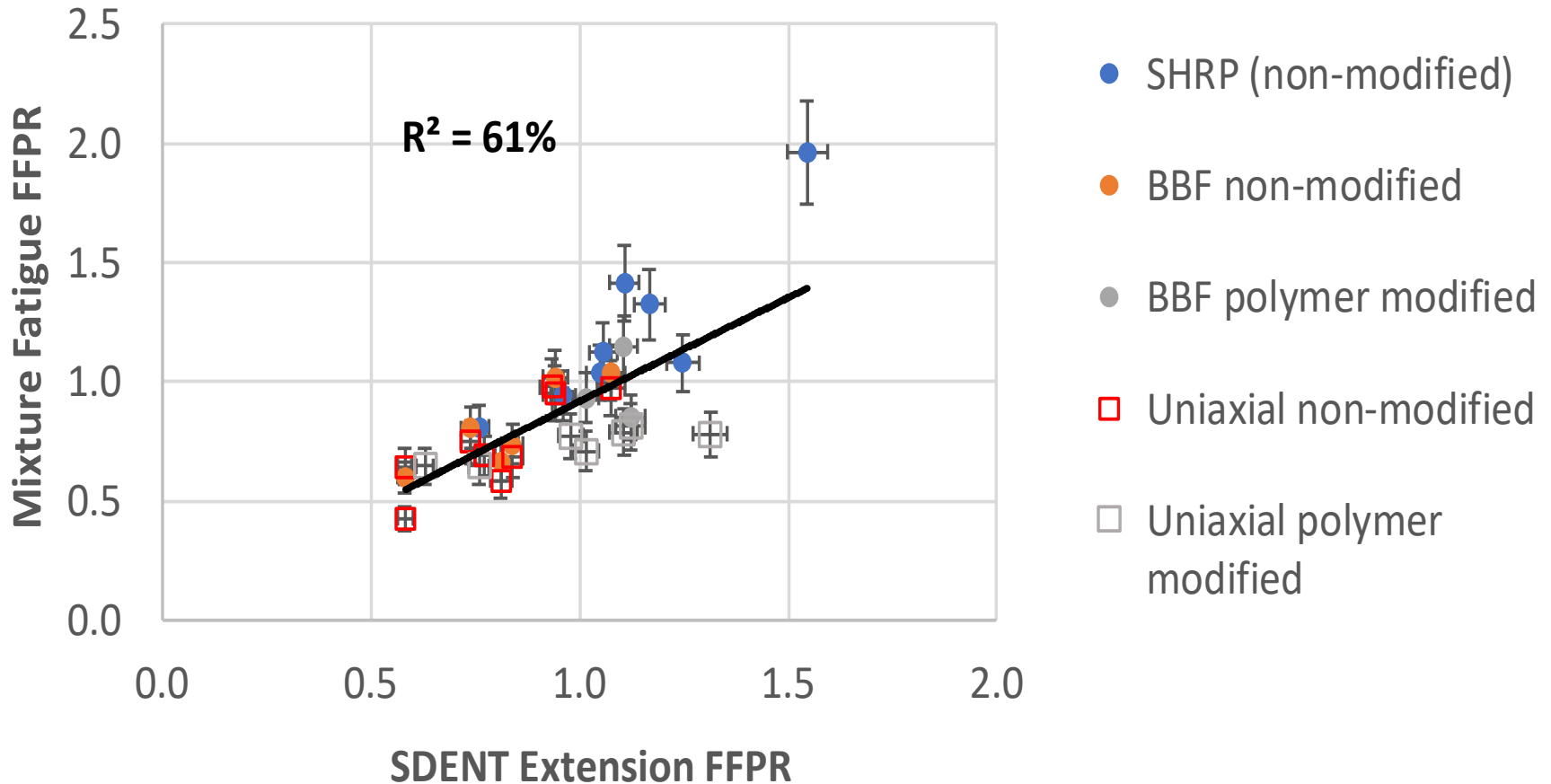
ENT/Extension FFPR and Binder R-value



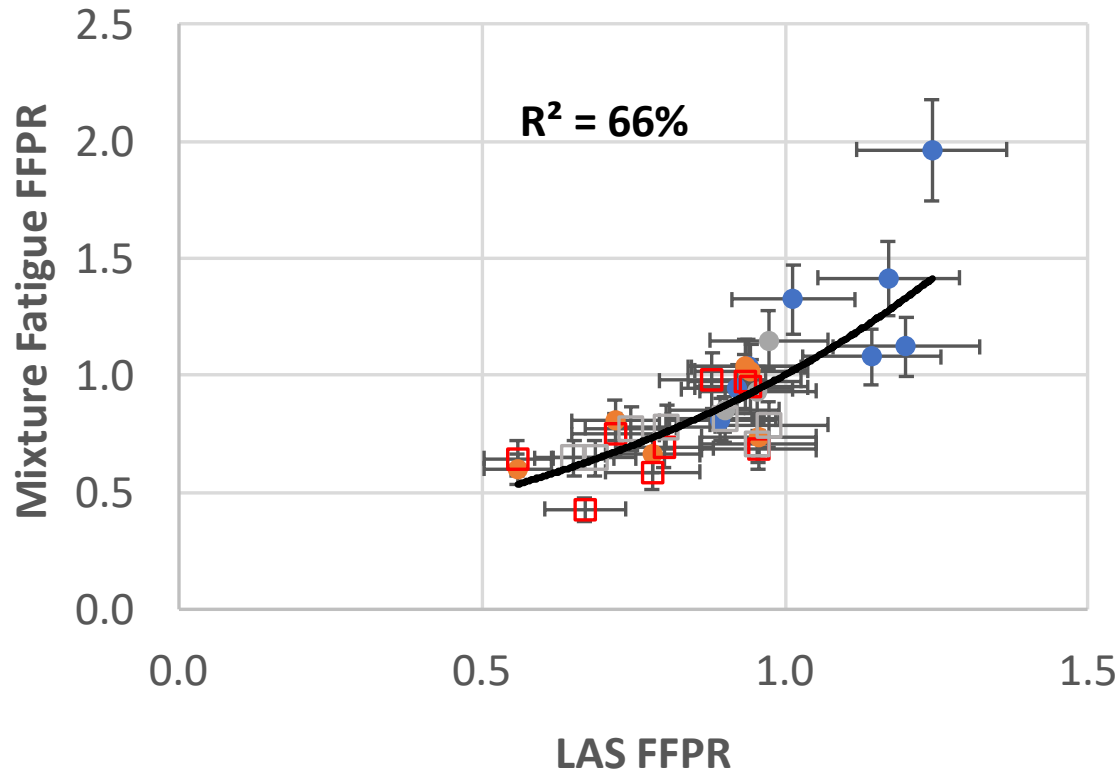
- SHRP (non-modified)
- NCHRP 9-59 non-modified
- NCHRP 9-59 polymer-modified



Mixture fatigue FFPR vs DENT/Extension FFPR



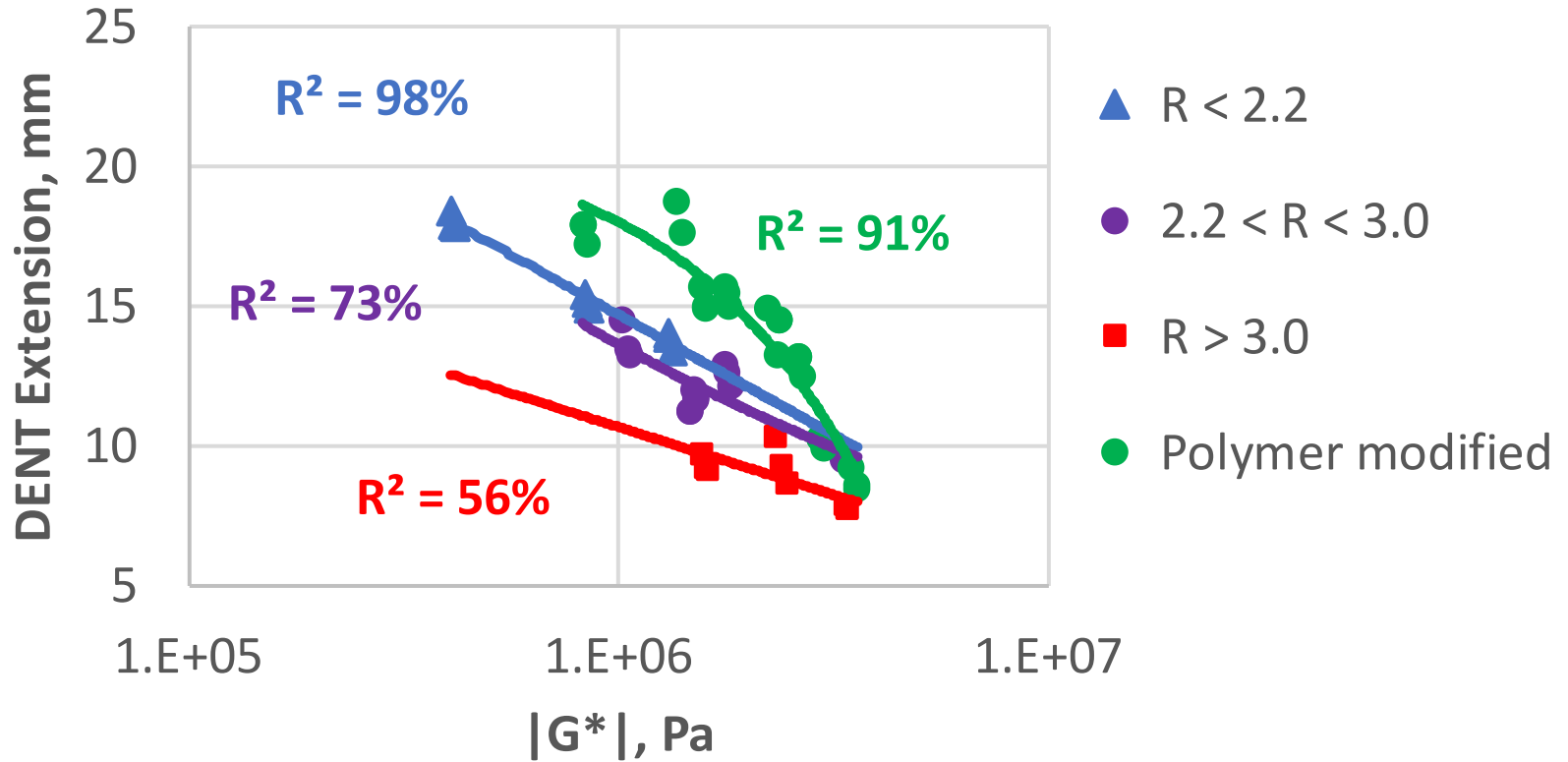
Mixture fatigue FFPR vs LAS FFPR



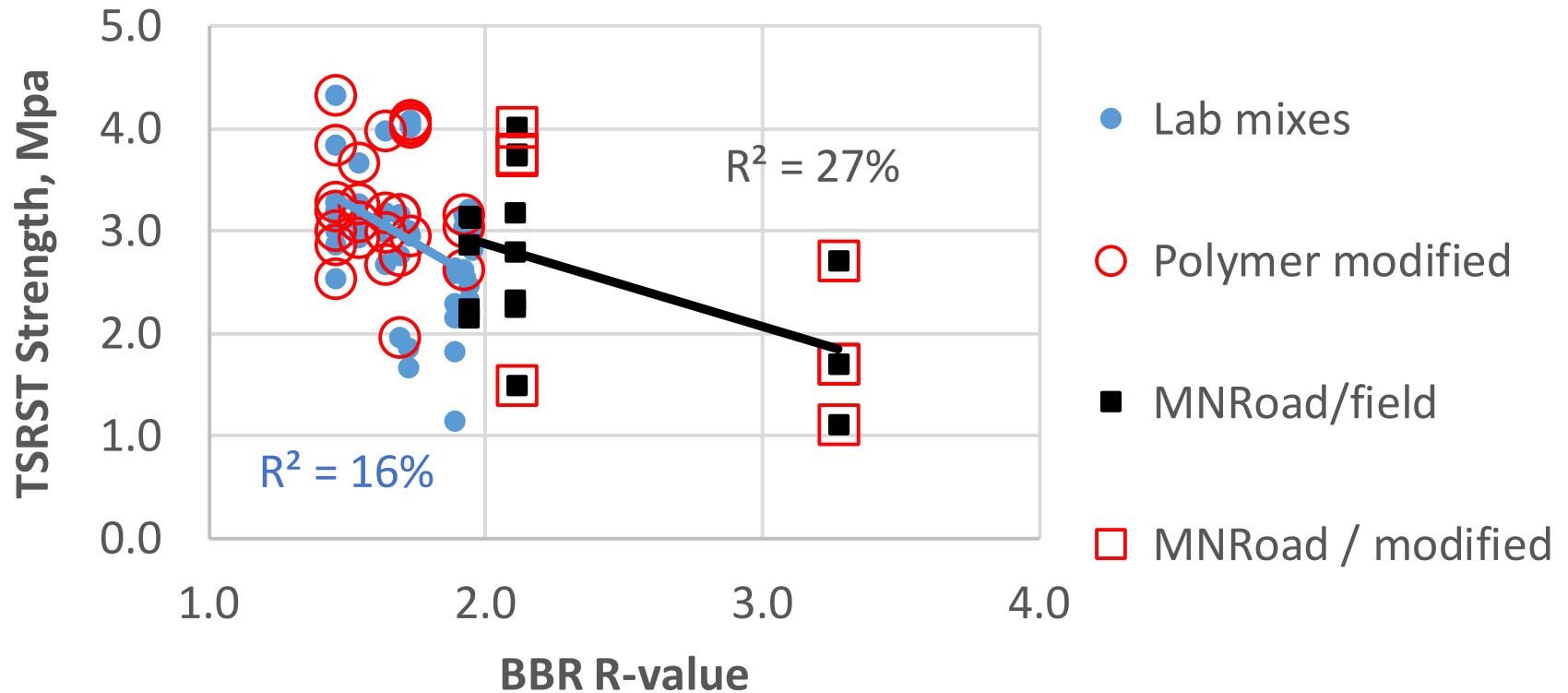
- SHRP (non-modified)
- BBF non-modified
- BBF polymer modified
- Uniaxial non-modified
- Uniaxial polymer modified



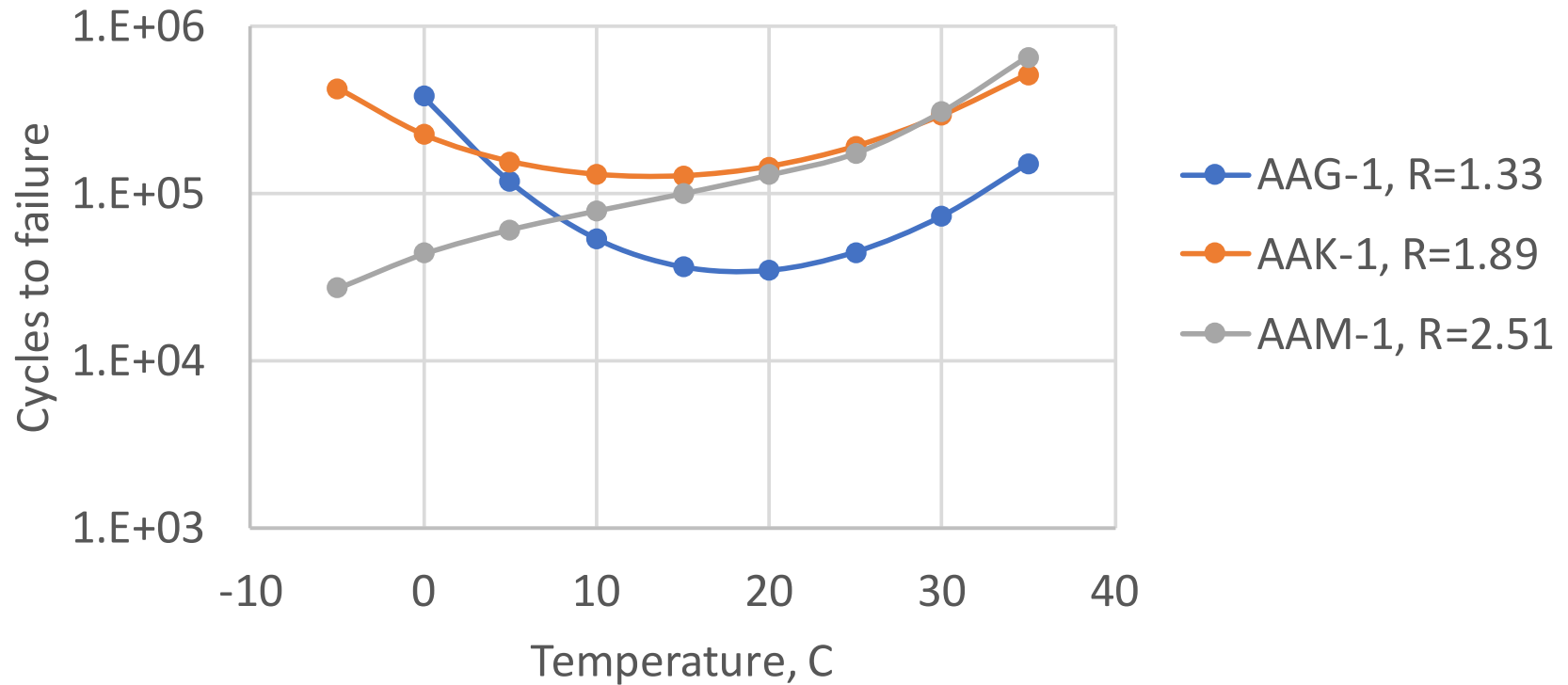
DENT extension vs G^*



NPFS 776: TSRST Strength and R-value



Pavement fatigue life and R-value



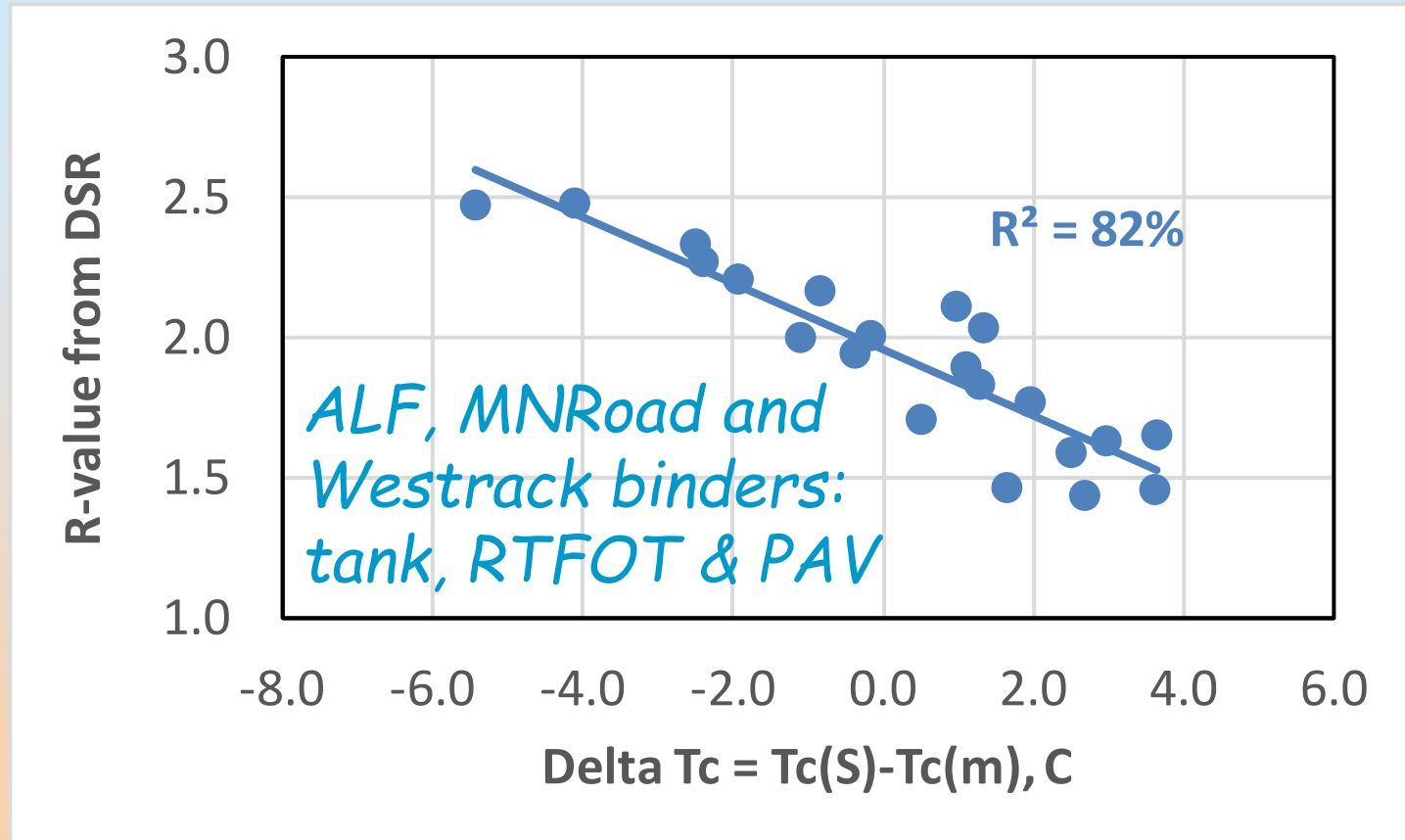
Simple LEA analysis with constant sub-base/sub-grade properties, 100-mm pavement



What about ΔT_c ? Glover-Rowe
Parameter? DENT test? Extended
BBR/physical hardening?



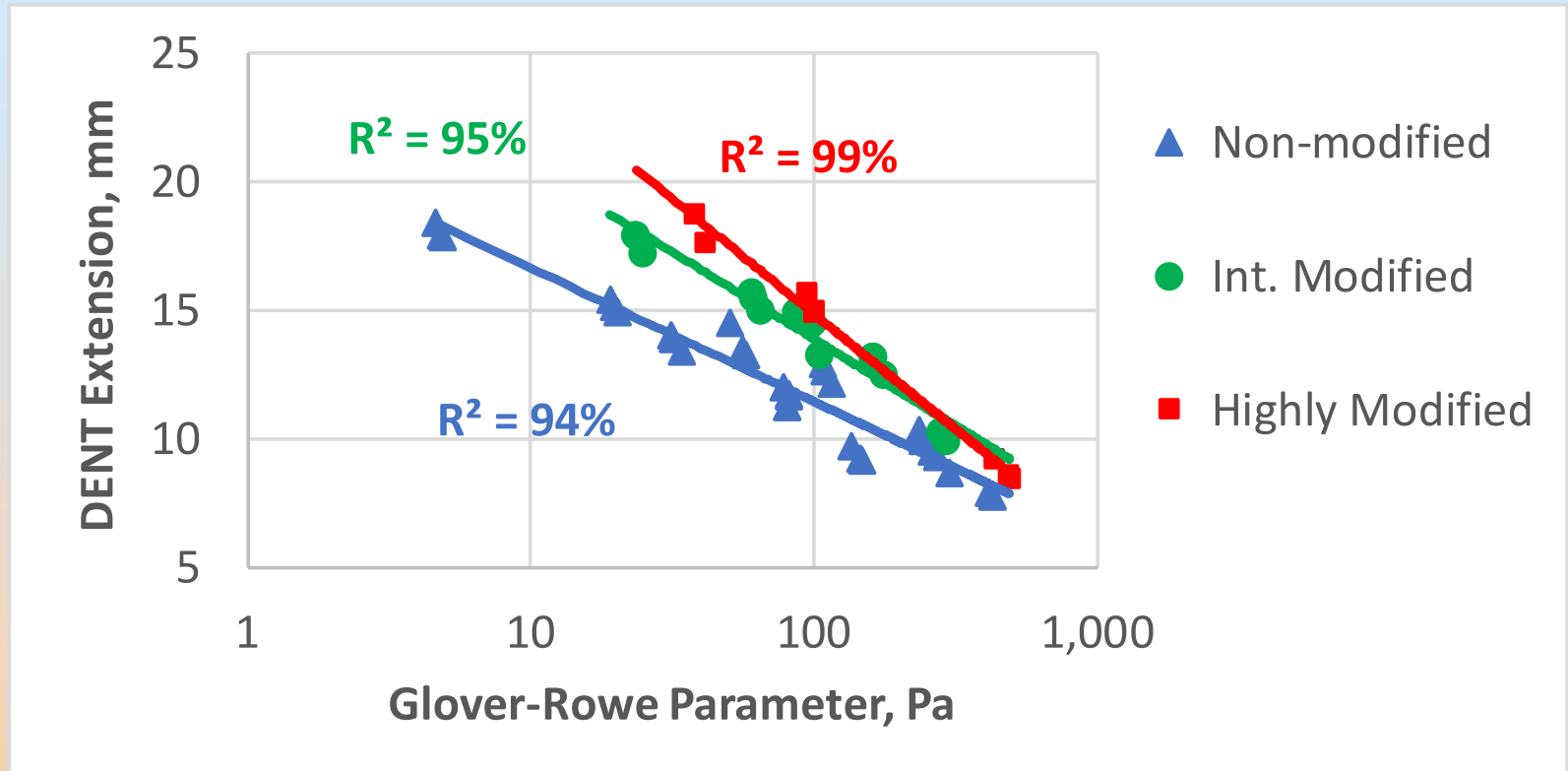
ΔT_c and R-value



ΔT_c and R-value are directly related, and both indicate rheologic type and strain tolerance



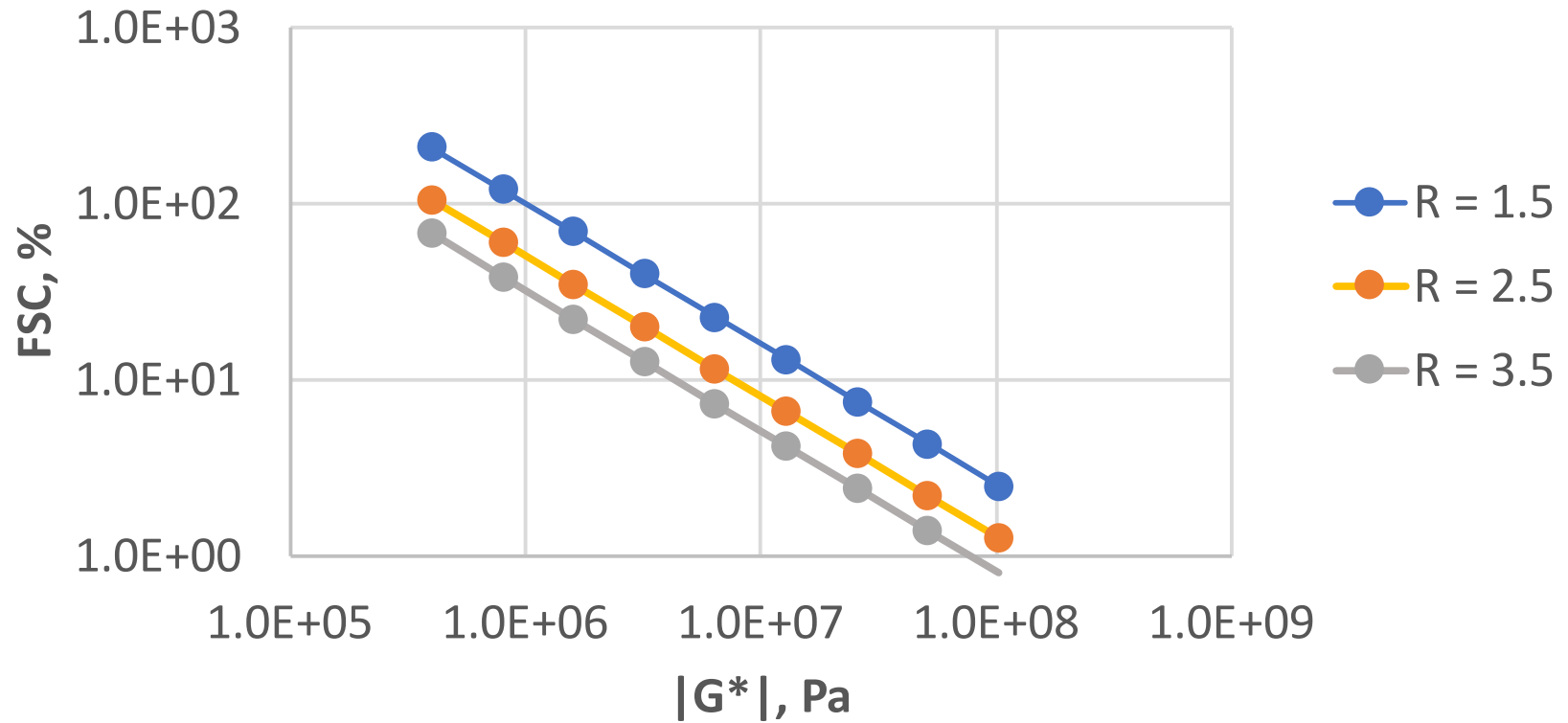
GRP and DENT extension



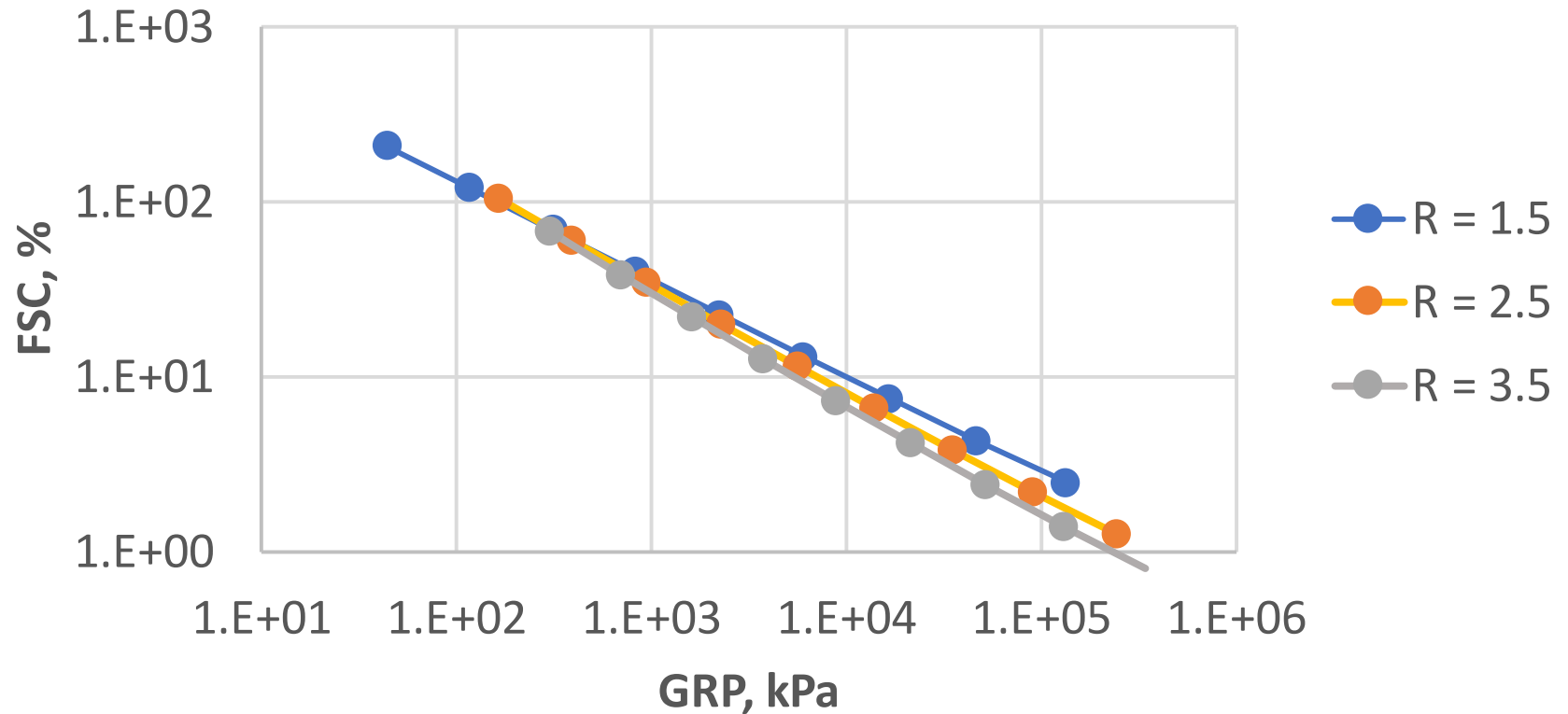
Of all rheological parameters examined, GRP has the best correlation to DENT extension



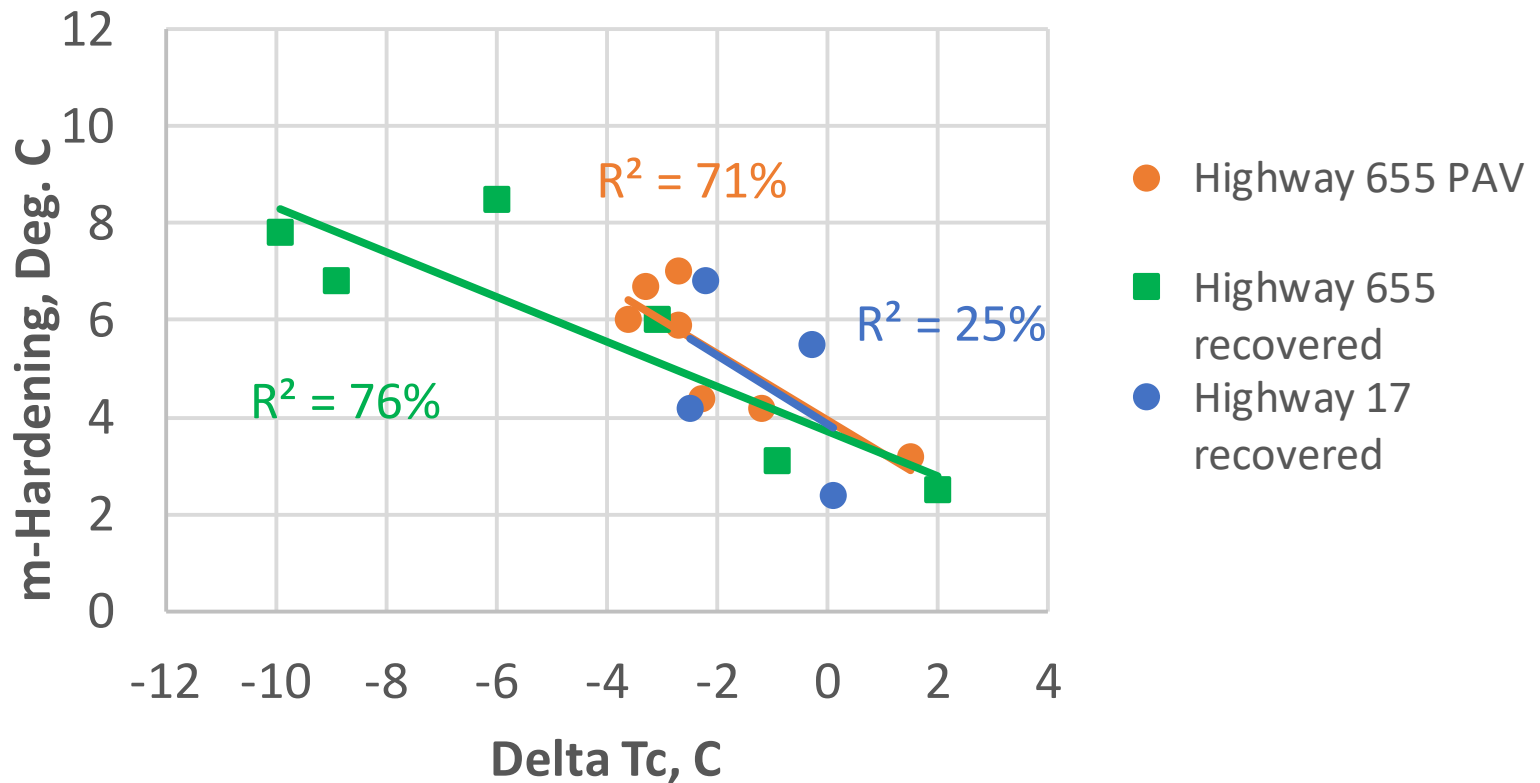
Modulus, R-value and FSC



GRP, R-value and FSC



Extended BBR/ physical hardening

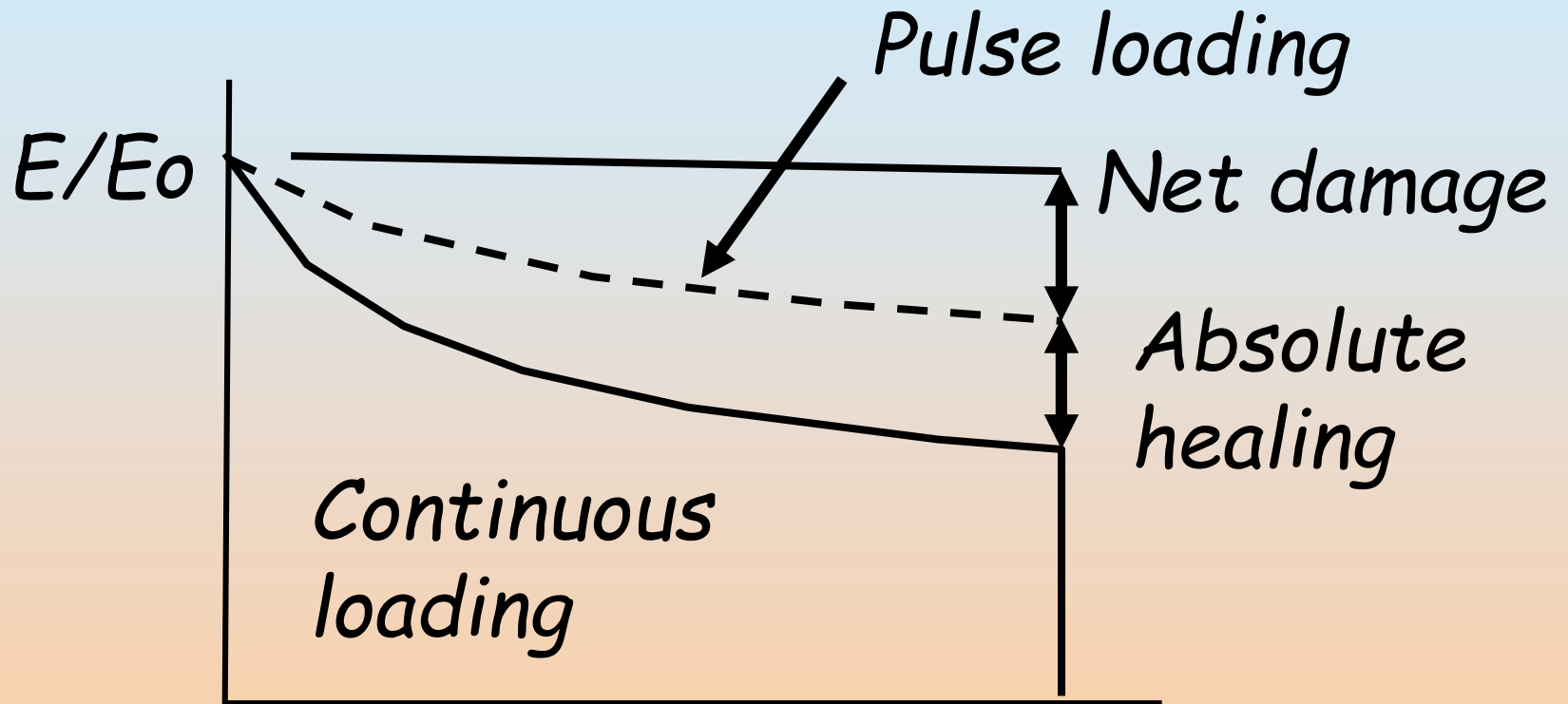


Extended BBR/ physical hardening

- Physical hardening increases with increasing ΔT_c / R-value
- For high $\Delta T_c/R$ the BBR will overestimate m-value
- Not only are these binders brittle, their BBR grades are lower than they should be...



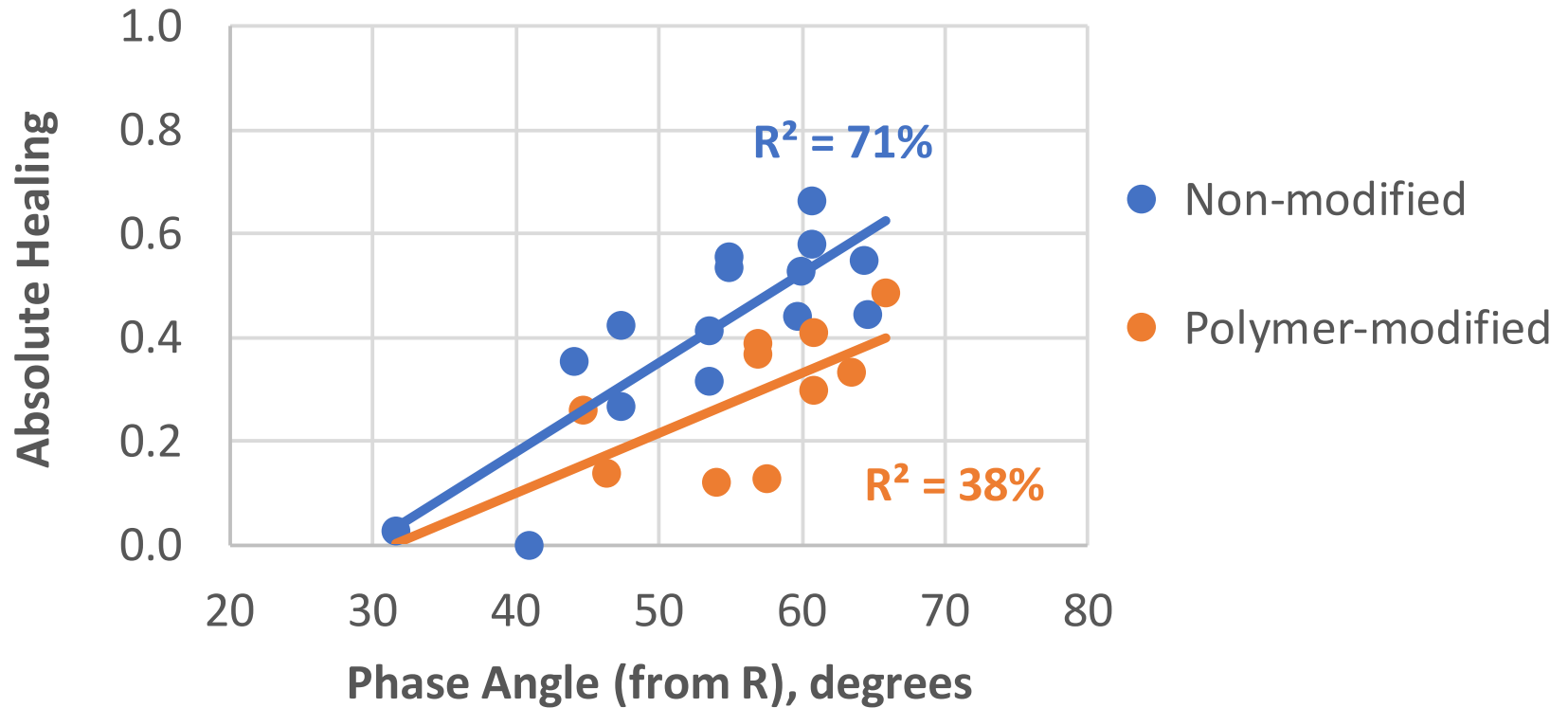
Adhesive healing



$$N_f \left[(FSC/\varepsilon_t) \times (VBE/100) \right]^{2.08(90/\delta)}$$



Adhesive Healing



Adhesive healing

- Absolute healing increases with increasing phase angle
- Since phase angle at a given modulus decreases with increasing R, binders with high R values will show less healing
- Maximum net damage at 10 to 20 MPa, increases with increasing R



Rheologic type can be specified in several ways

- R-value

- Calculated from DSR, G^* apx. 10 Mpa
- Calculated from BBR

- DSR minimum phase angle at $G^* = 10$ MPa for example

- BBR, maximum S at m 0.3, for example

- BBR, maximum ΔT_c



Polymer-modified binders

- High R-values appear to be as bad or worse for the performance of polymer-modified binders as for non-modified ones
- Probably need similar control of R for all binders
 - Level of modification should be controlled primarily through high temperature spec



Summary

- Binders with high R-values are a “triple whammy”
 - Increased brittleness
 - Decreased adhesive healing
 - Errors in BBR grading
- Need to control rheologic type-- ΔT_c , R-value or some related parameter—to eliminate these problems



Remaining work

- Draft final report is being compiled
- Completion of validation testing
- Related work being done as part of NCHRP 9-60 (binder manufacture/pavement performance/specifications) and NCHRP 9-61 (binder aging)



Acknowledgements

- NCHRP
- The Project Panel
- Industry suppliers
- Nam Tran and his associates at NCAT
- My associates at AAT

