

DSR testing of GTR

Particle size effects

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- Crumb rubber sizes
 - #16-#20 (~1mm)
 - #20-#30 (~0.7 mm)
 - #40-#50 (~0.4 mm)
- Crumb rubber percentages
 - 15%, 20%, 25%
- Test geometry
 - Parallel plate
 - Concentric cylinders
- PG58-28 base binder

Sample preparation (wet process)

- Mixing temperature:
190C \pm 5C
- Mixing duration: 1 hr
- Mixing speed: 1000 RPM
- Two to three replicate
batches



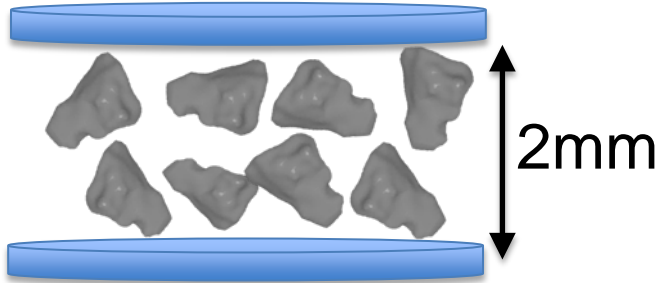
- 25 mm plate
 - $T = 46, 58, 70, \text{ and } 82^{\circ}\text{C}$
 - $\omega = 10, 15.84, 25.12, 39.81, 63.09, 100 \text{ rad/s}$
 - 2 mm gap
- 8 mm plate
 - $T = 15 \text{ and } 30^{\circ}\text{C}$
 - $\omega = 10, 15.84, 25.12, 39.81, 63.09, 100 \text{ rad/s}$
 - 2 mm gap



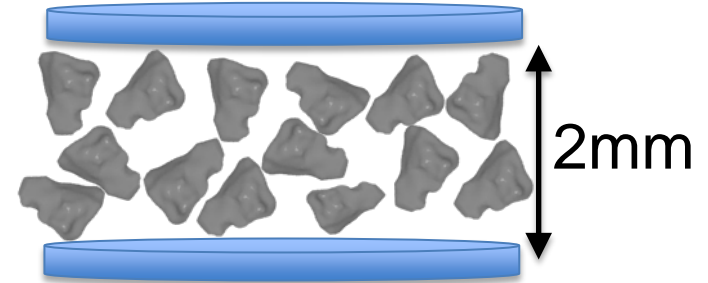
Effect of Crumb Rubber size

At different percentages of rubber

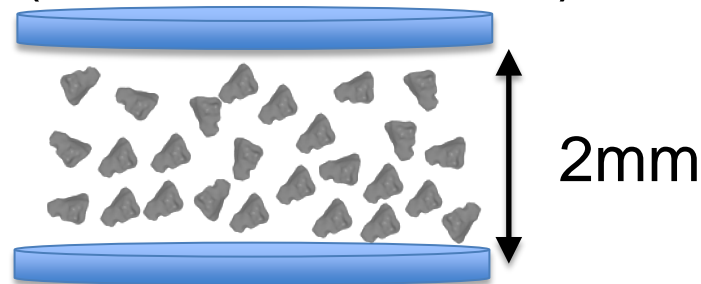
#16-#20
(1.18 - 0.85 mm)



#20 - #30
(0.85 - 0.6 mm)

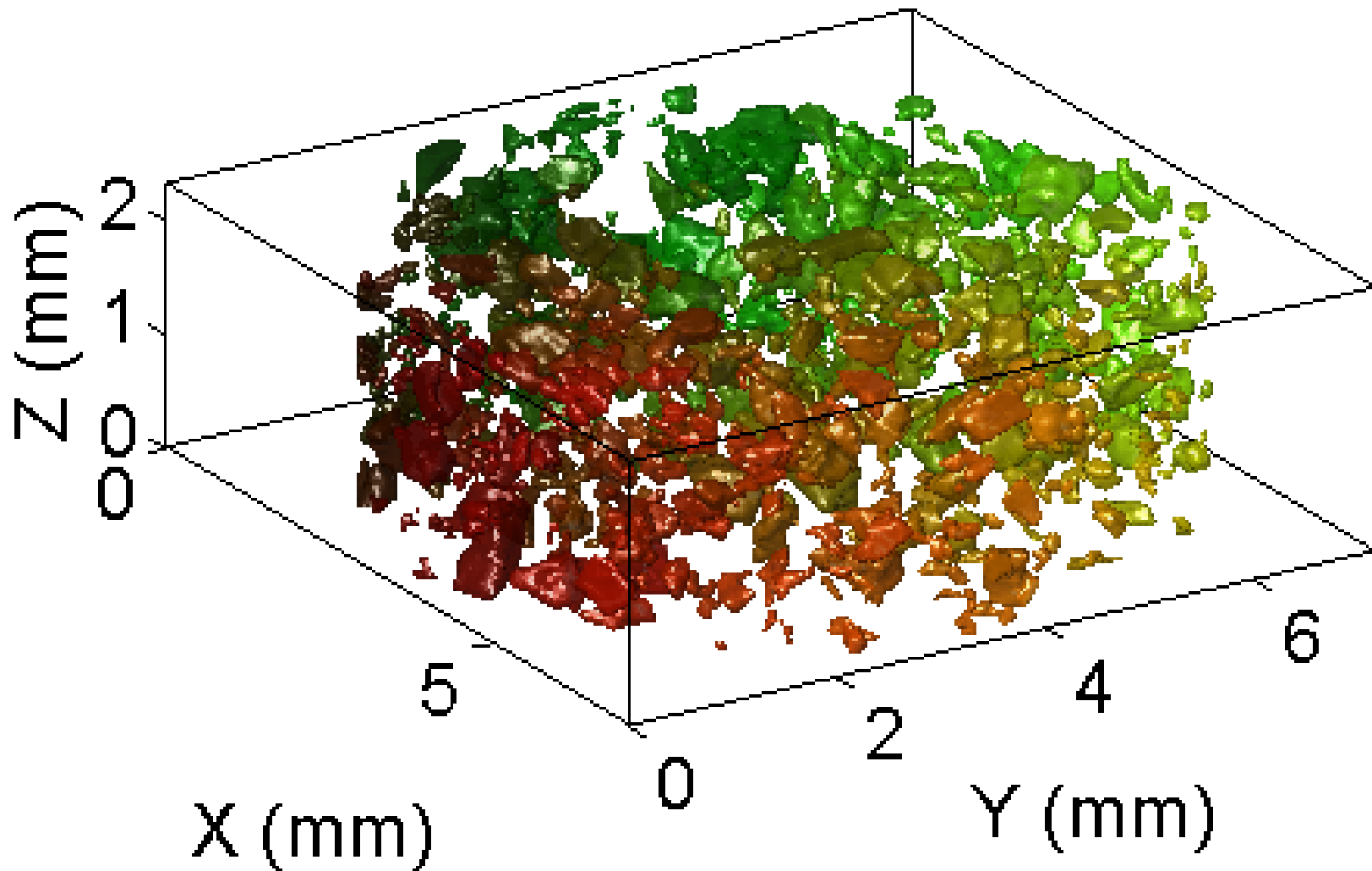


#40-#50
(0.425 - 0.355 mm)



X-ray CT of 15% CR

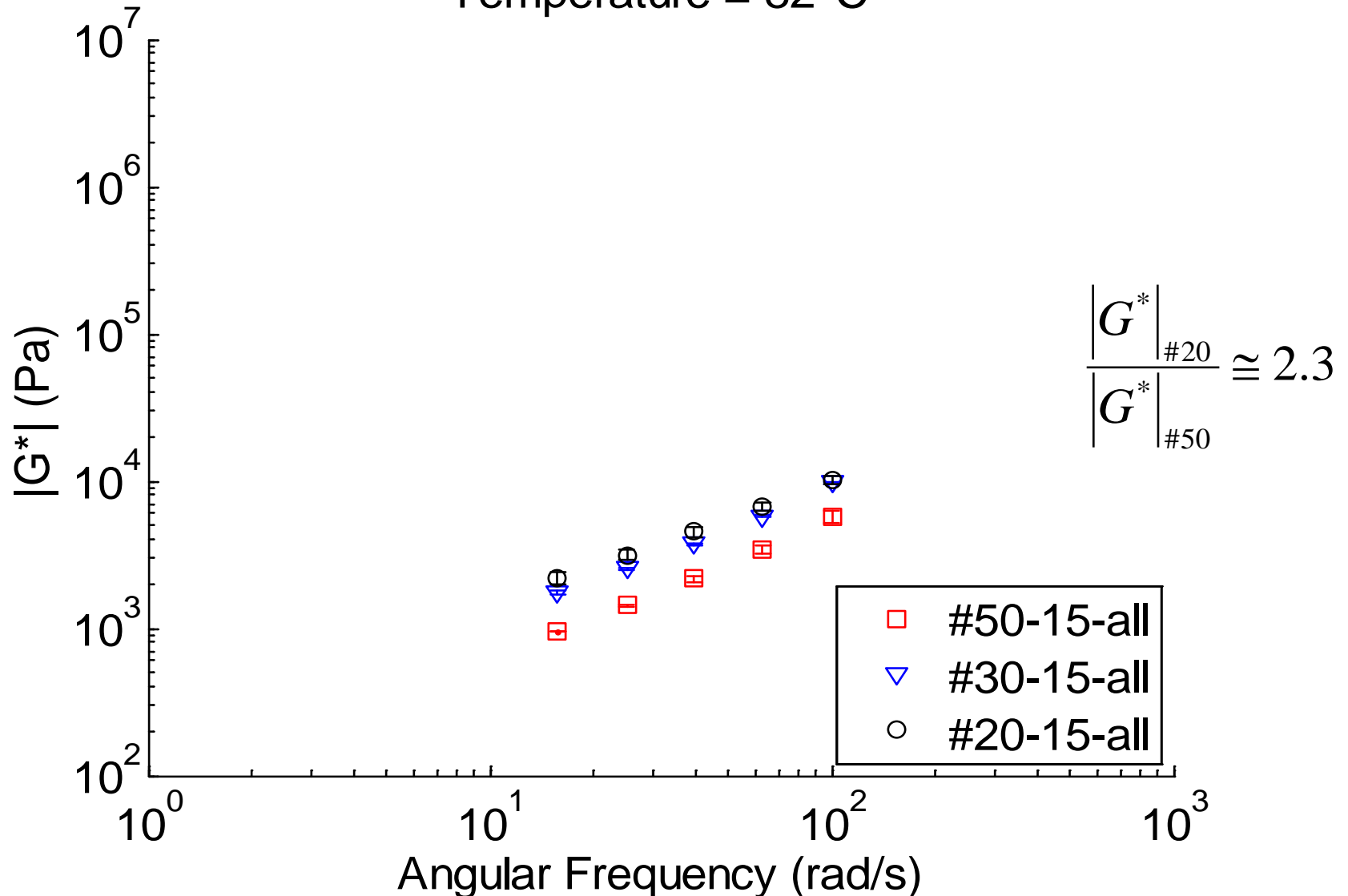
CR passing #30, retaining #40 sieve



Effect of CR size

- For 15% CR content (by binder weight)

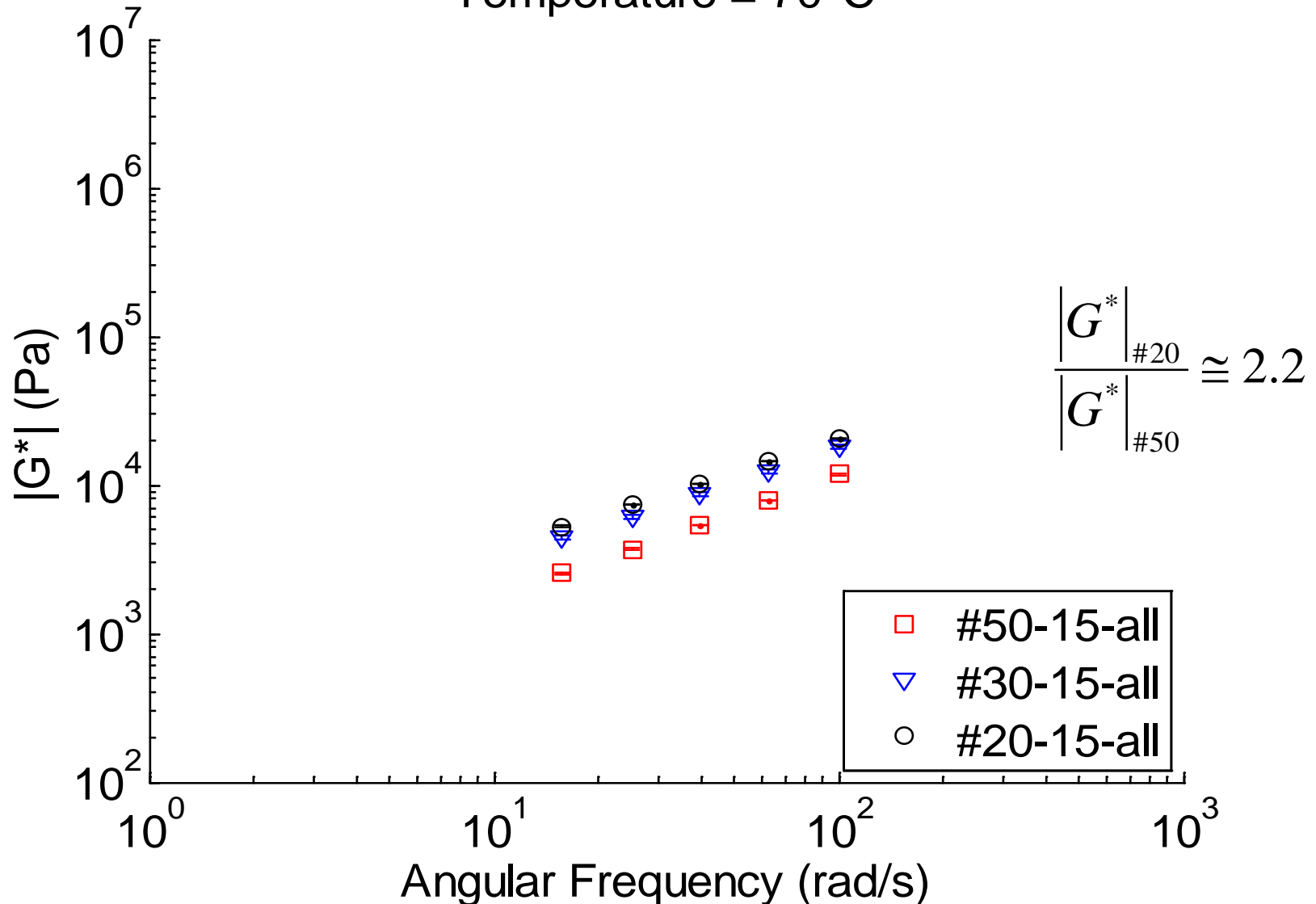
Temperature = 82°C



Effect of CR size

- For 15% CR content (by binder weight)

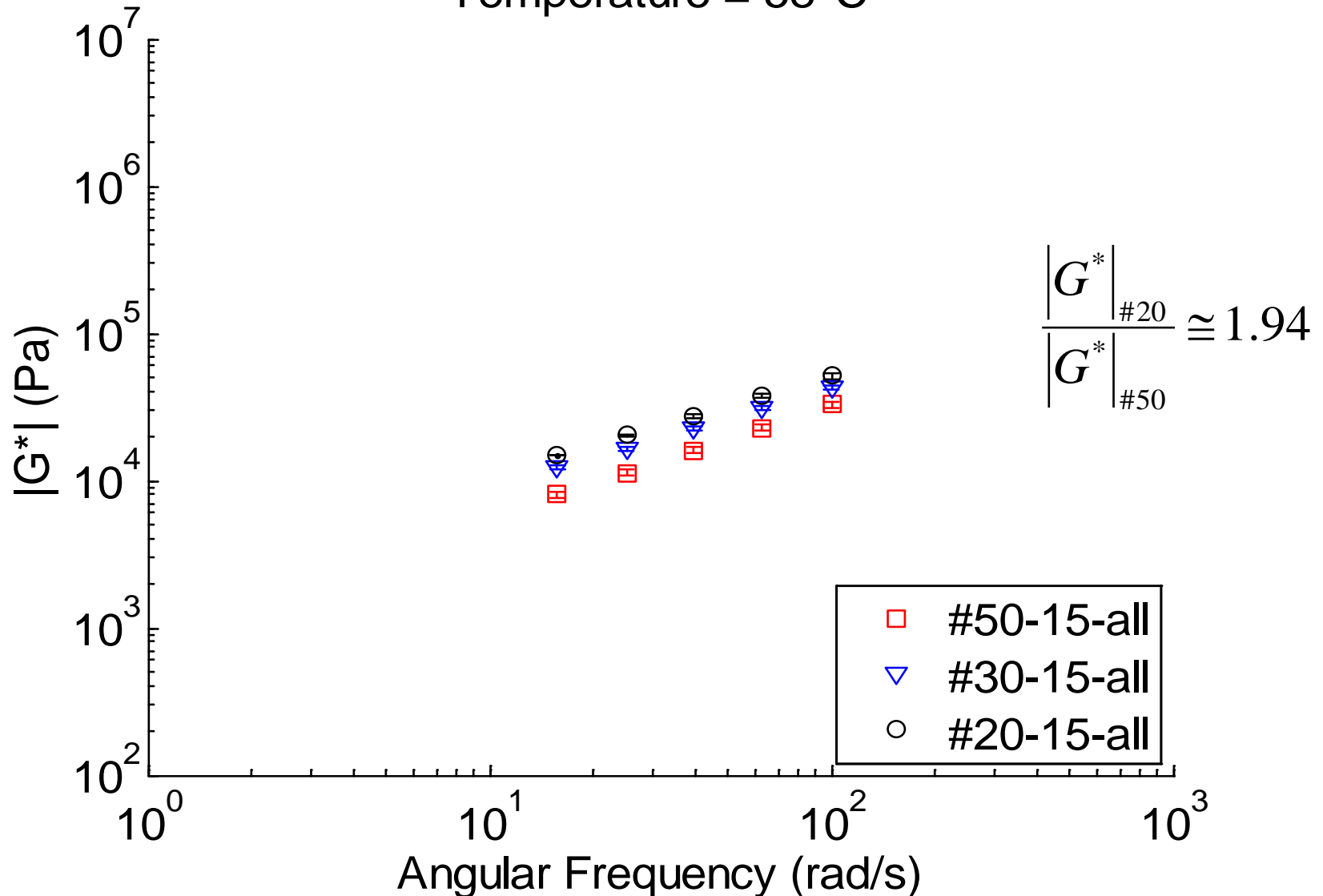
Temperature = 70°C



Effect of CR size

- For 15% CR content (by binder weight)

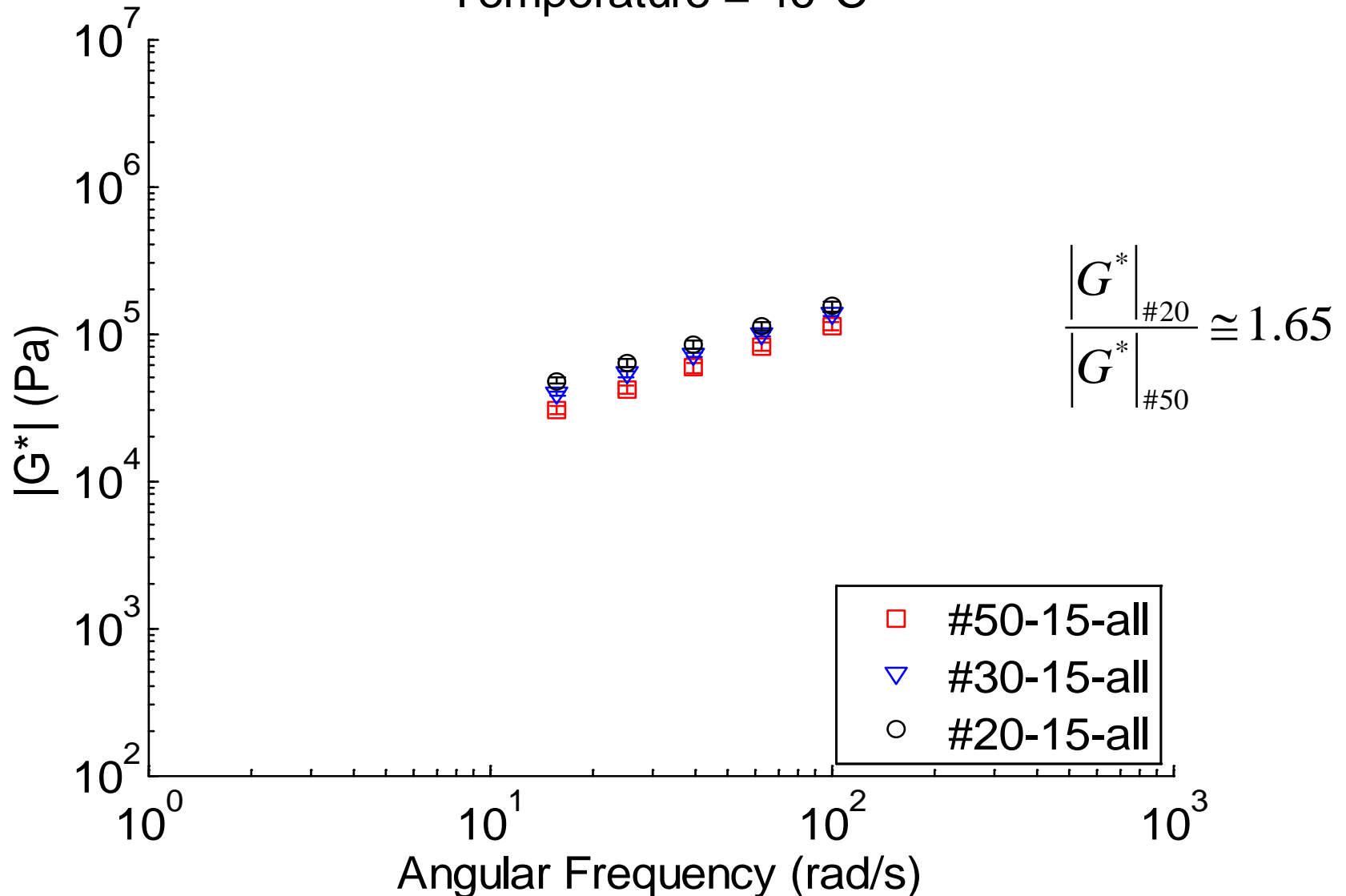
Temperature = 58°C



Effect of CR size

- For 15% CR content (by binder weight)

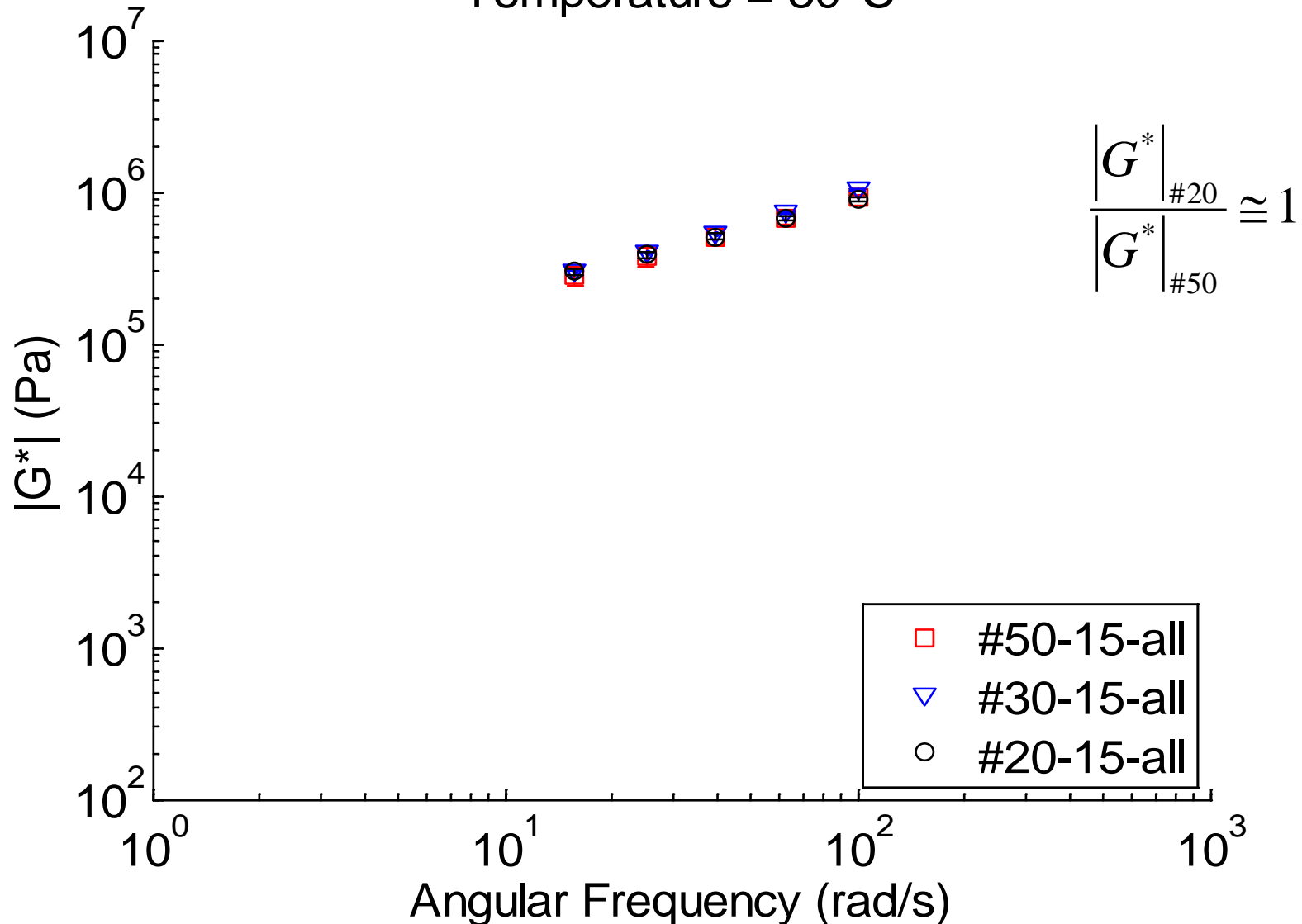
Temperature = 46°C



Effect of CR size

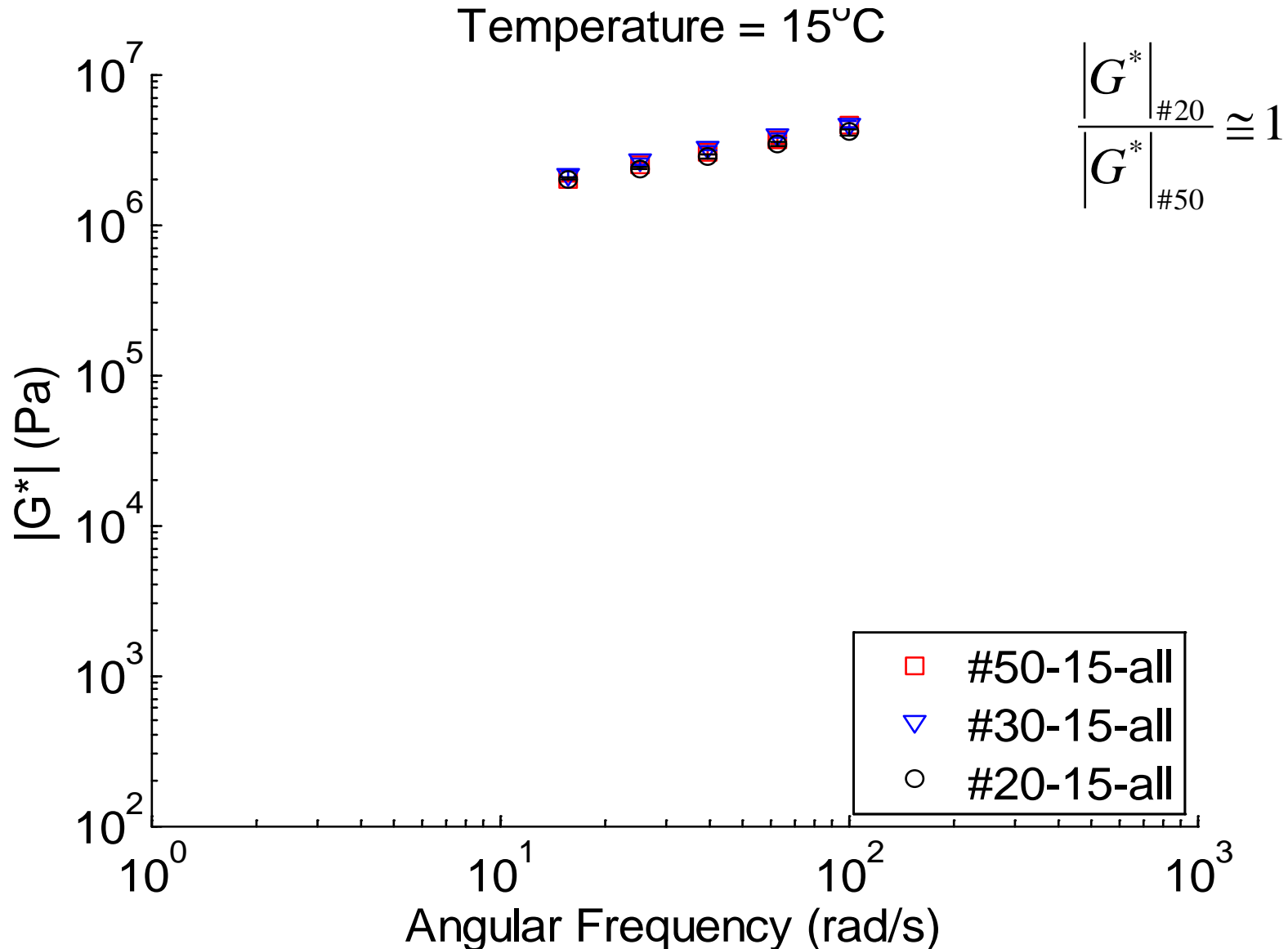
- For 15% CR content (by binder weight)

Temperature = 30°C

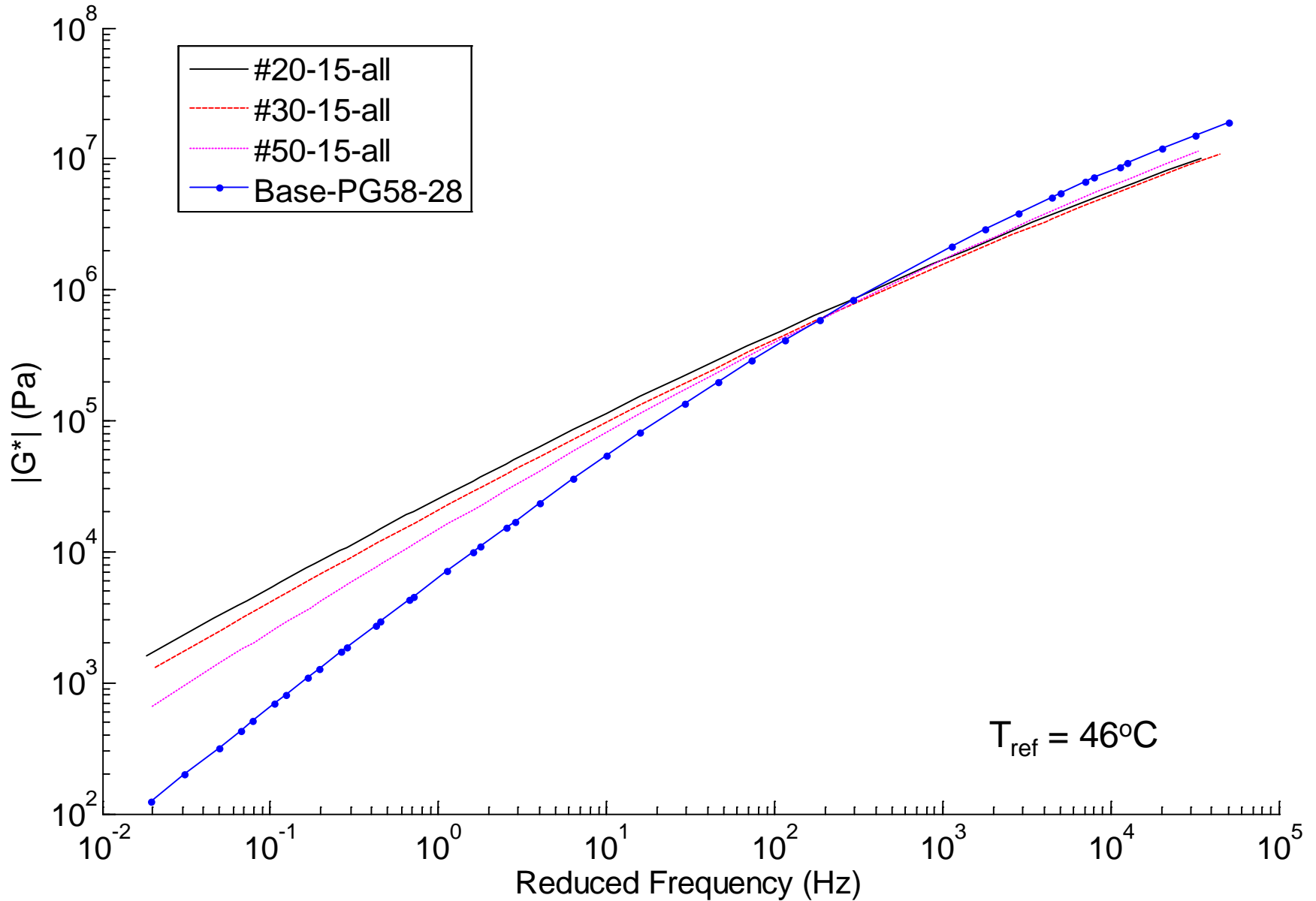


Effect of CR size

- For 15% CR content (by binder weight)



$|G^*|$ mastercurves (15% CR)

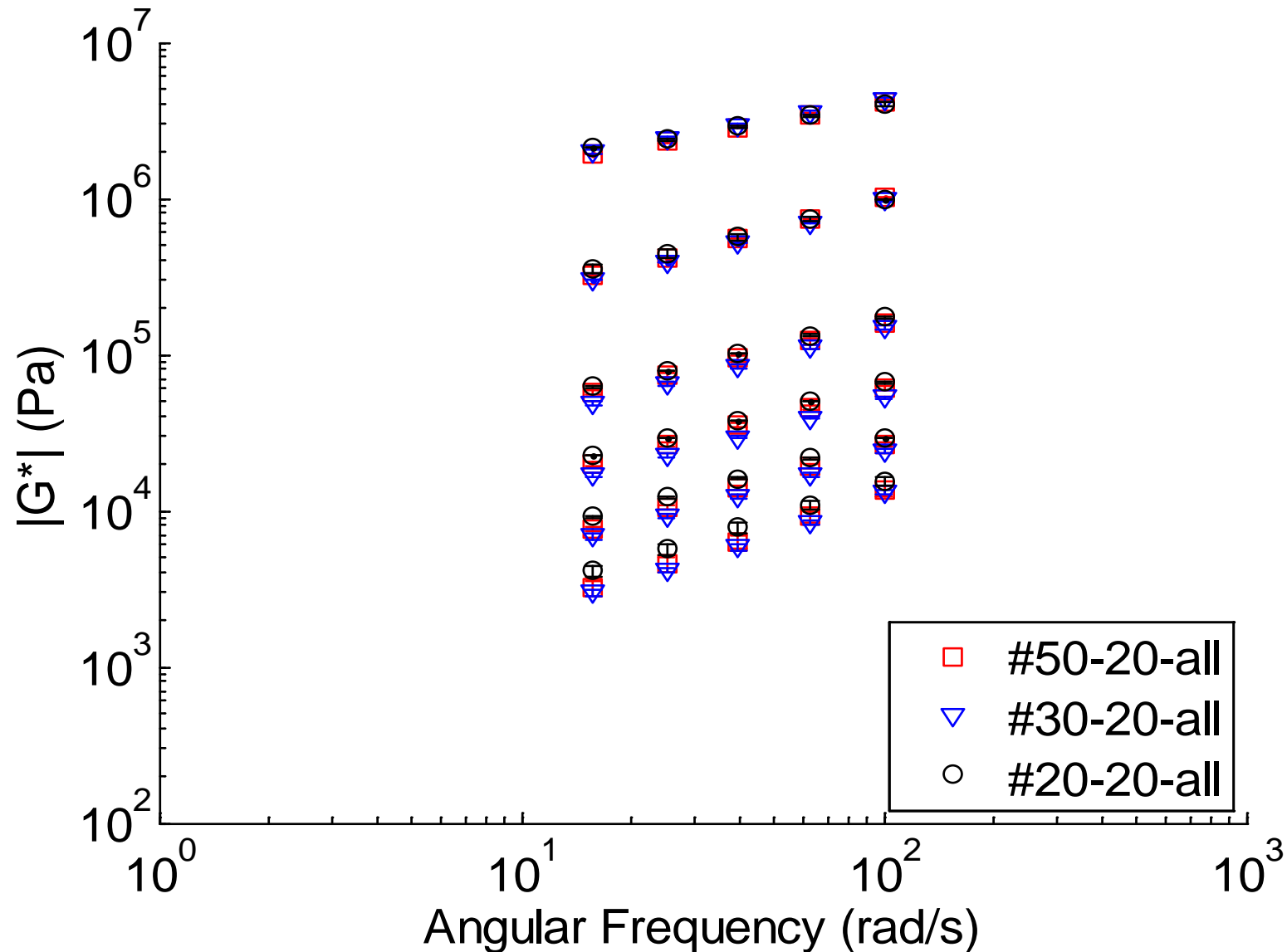


Effect of Crumb Rubber size

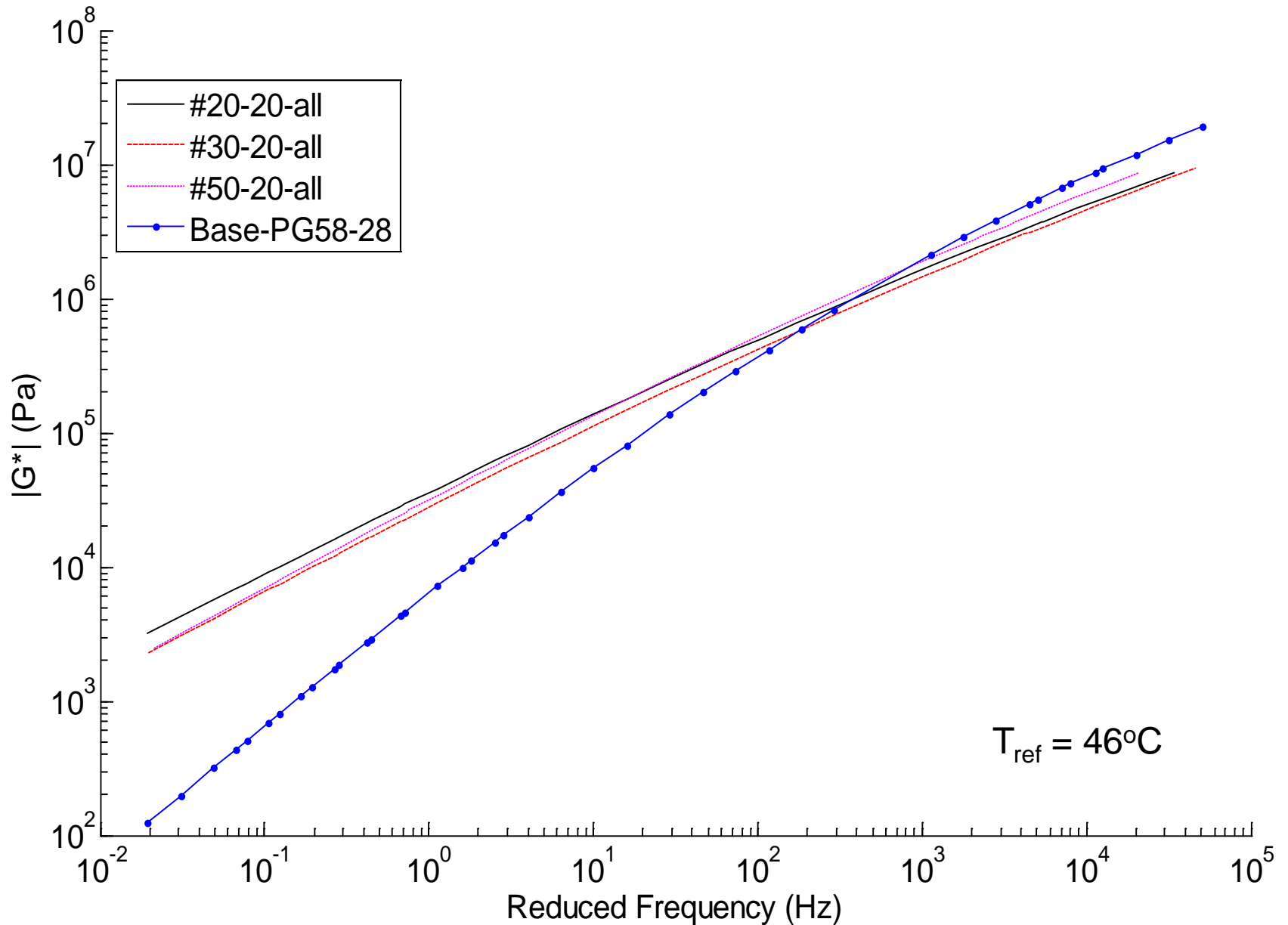
At 20% rubber

Effect of CR size

- For 20% CR content (by binder weight)



$|G^*|$ mastercurves (20% CR)

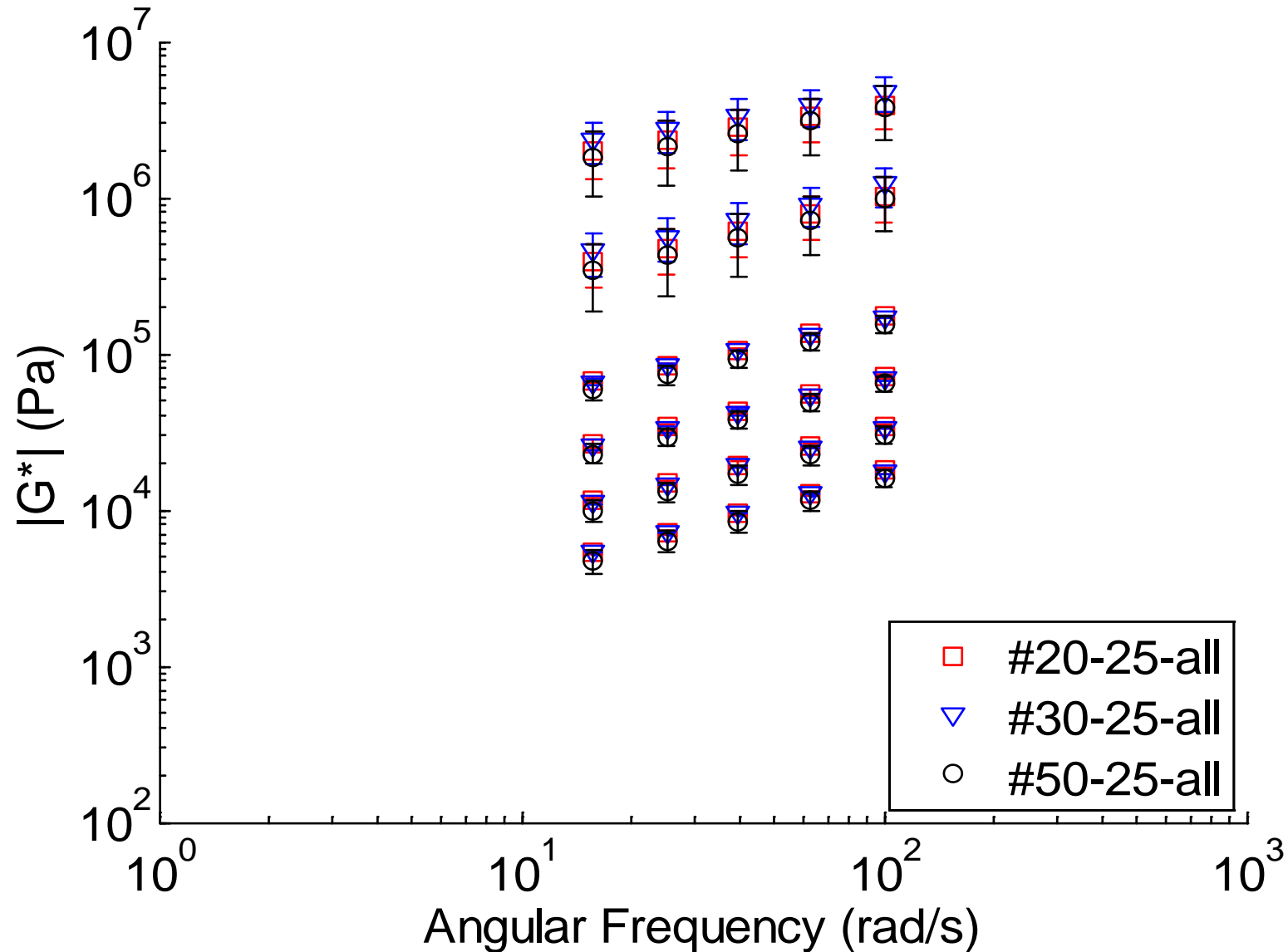


Effect of Crumb Rubber size

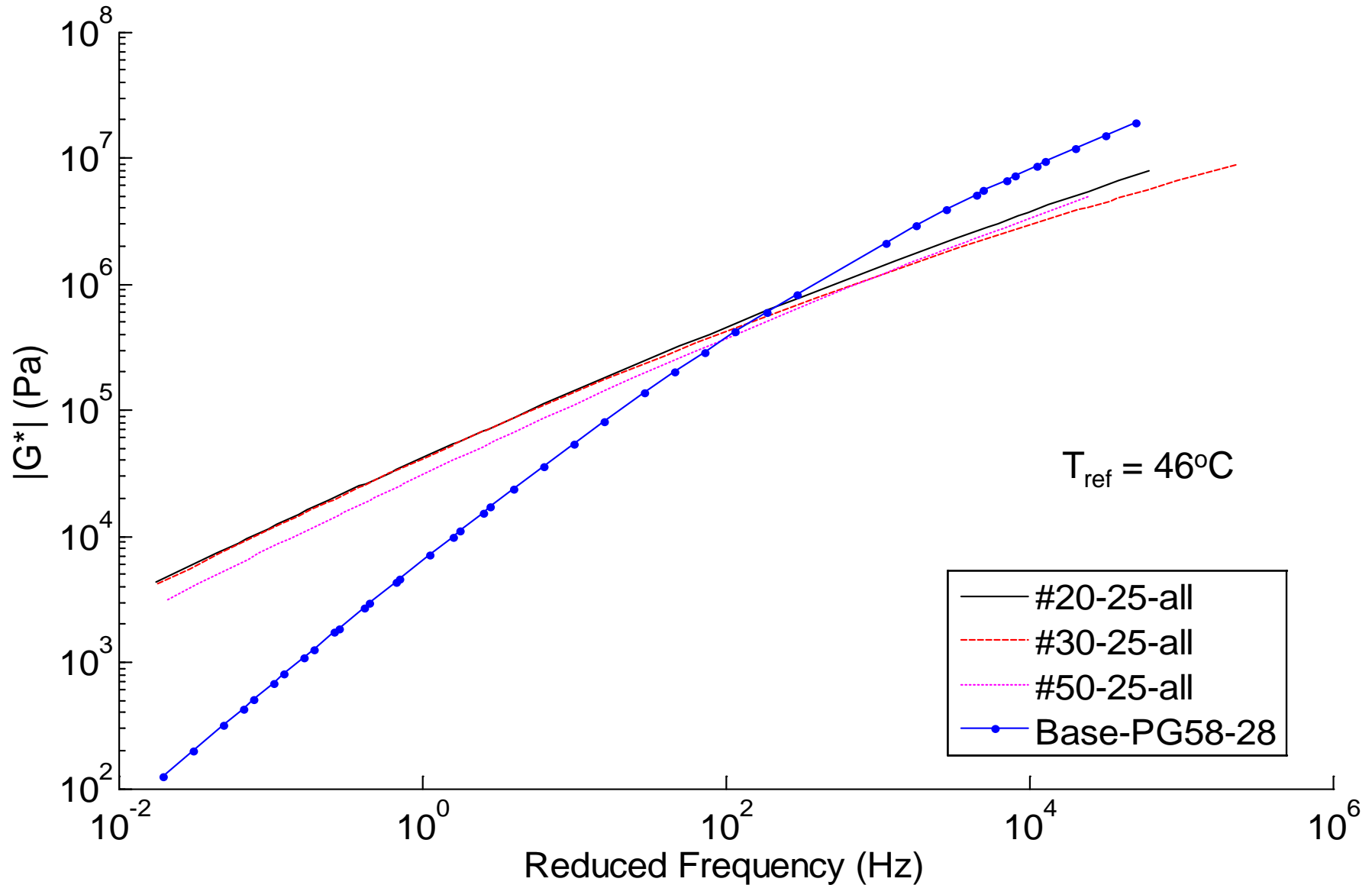
At 25% rubber

Effect of CR size

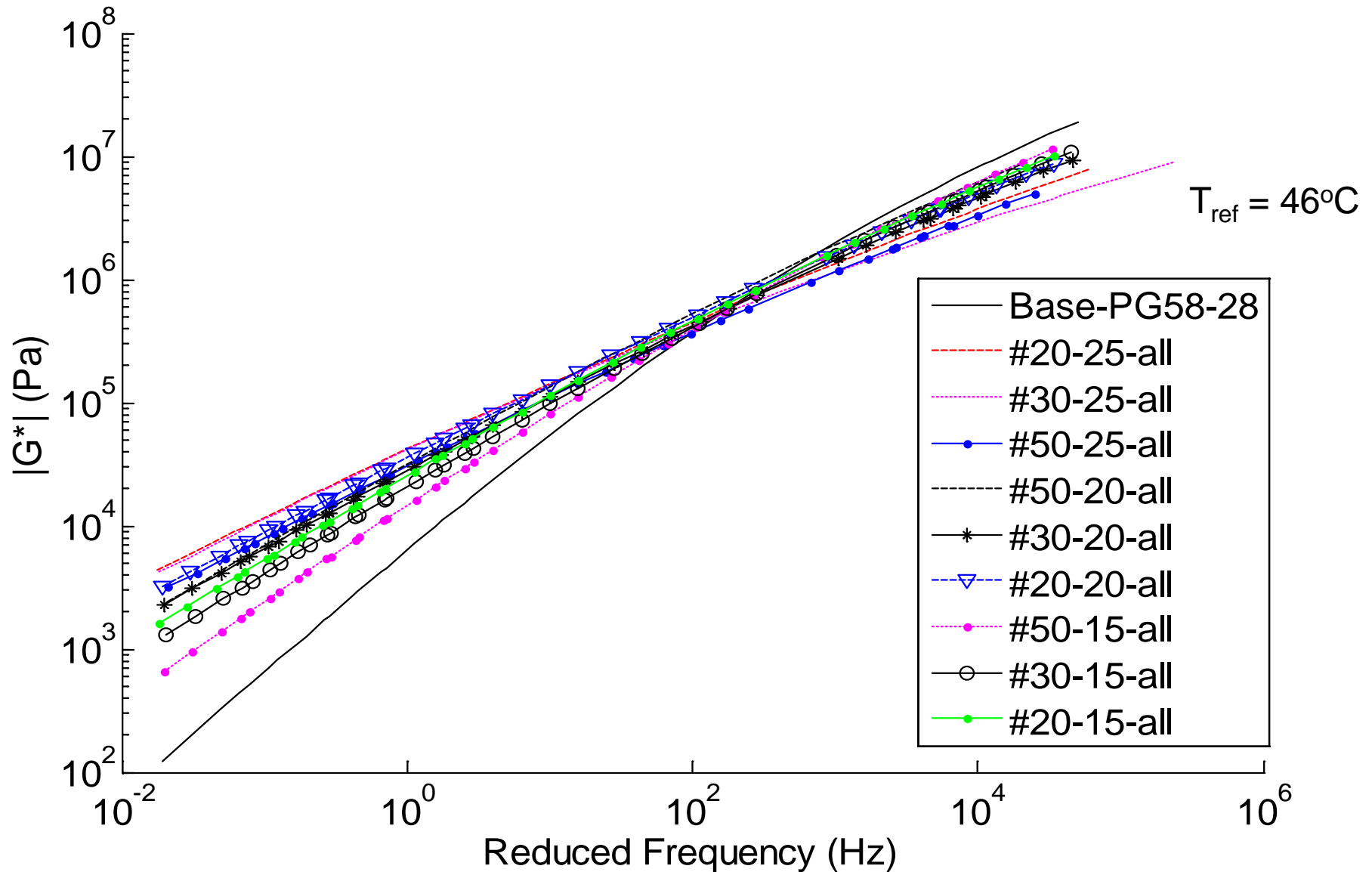
- For 25% CR content (by binder weight)



$|G^*|$ mastercurves (25% CR)

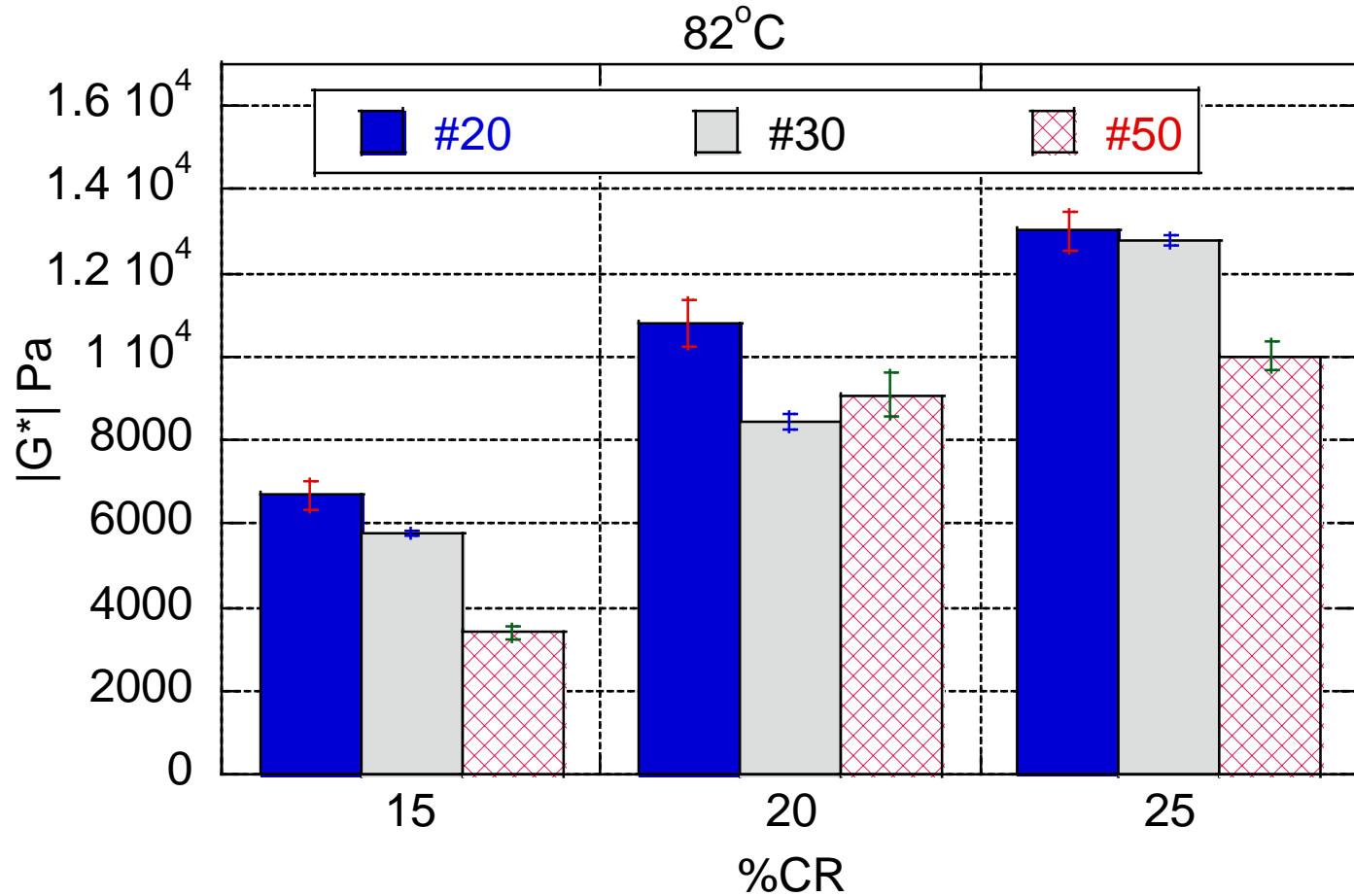


$|G^*|$ mastercurves (ALL sizes)



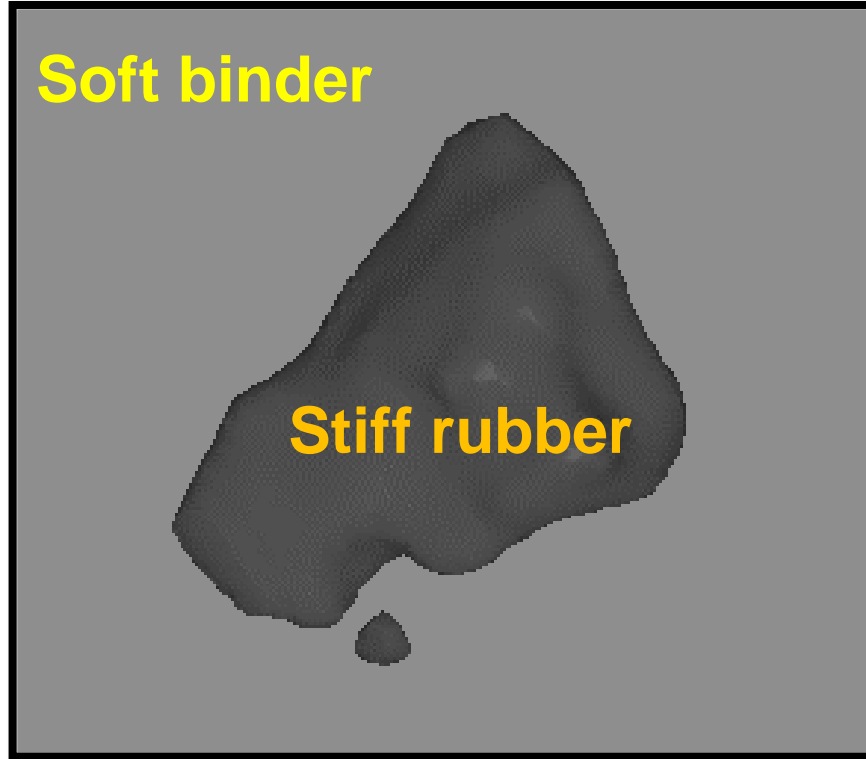
Effect of CR percentage & size

$|G^*|$ at 10Hz

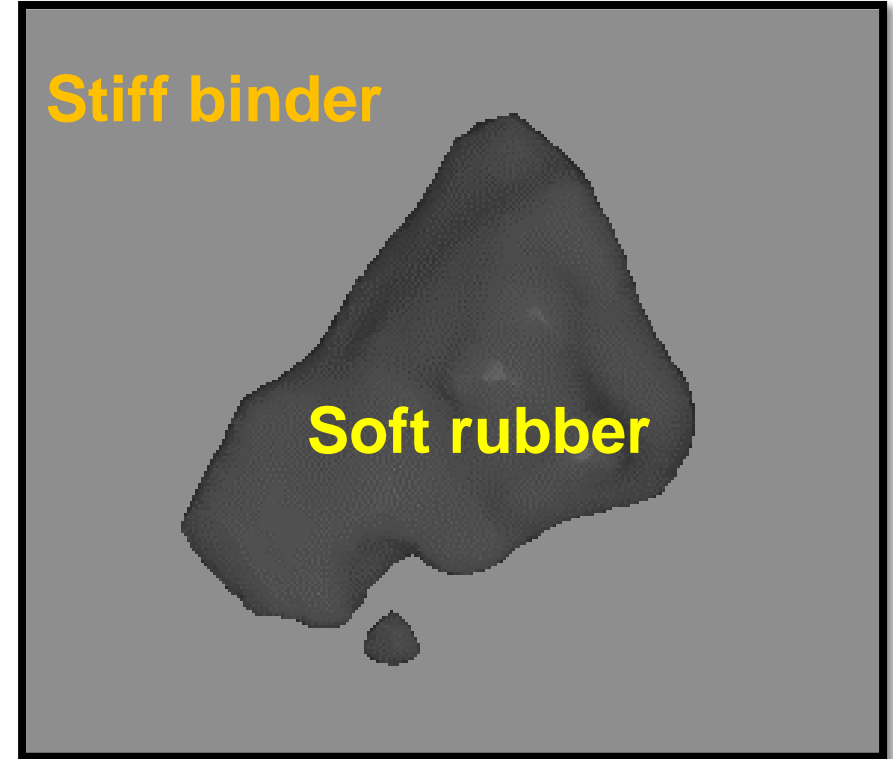


High T versus Low T

T = 76°C



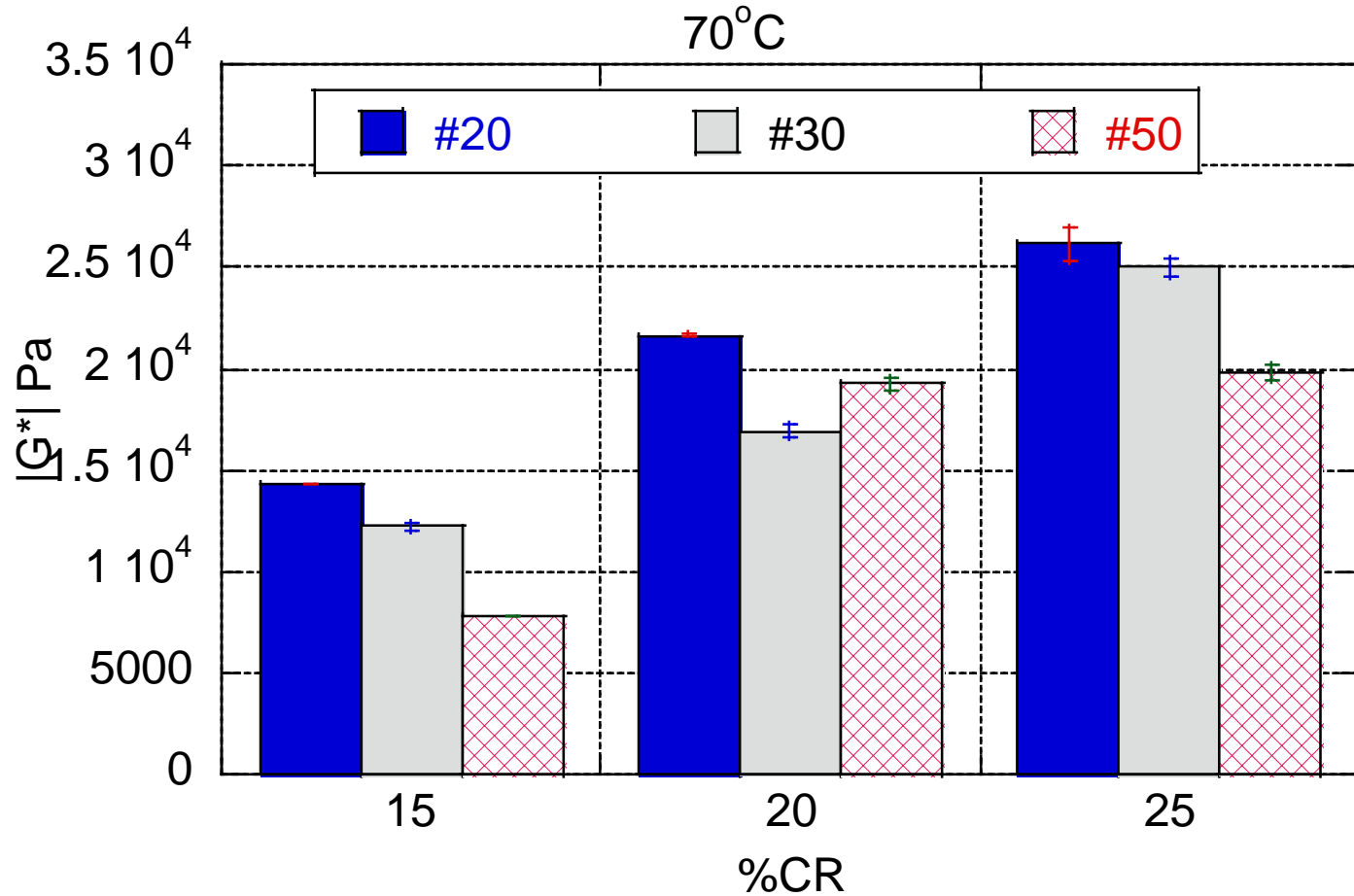
T = 15°C



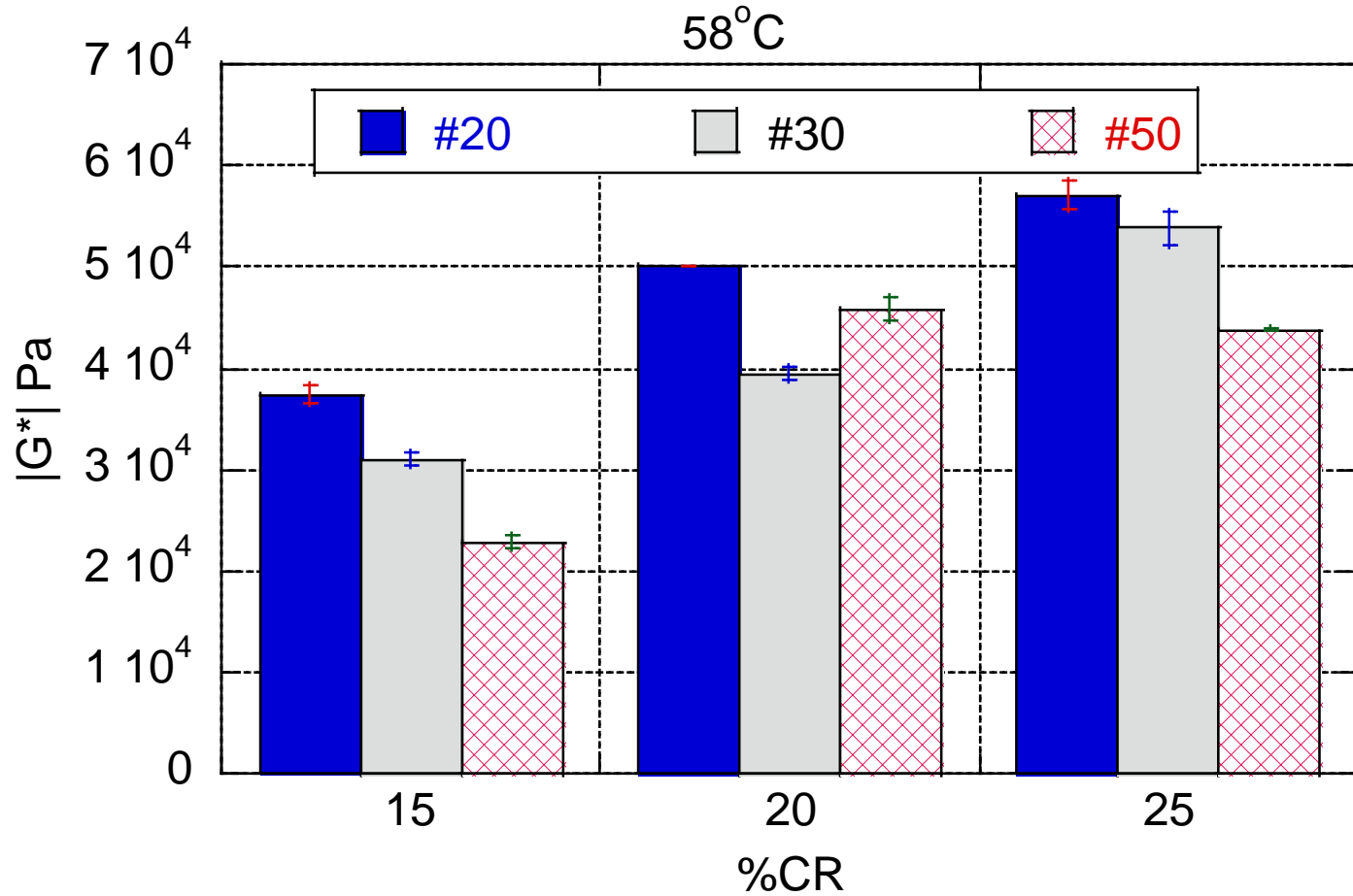
Rubber  $|G^*|$ of mix 

Rubber  $|G^*|$ of mix 

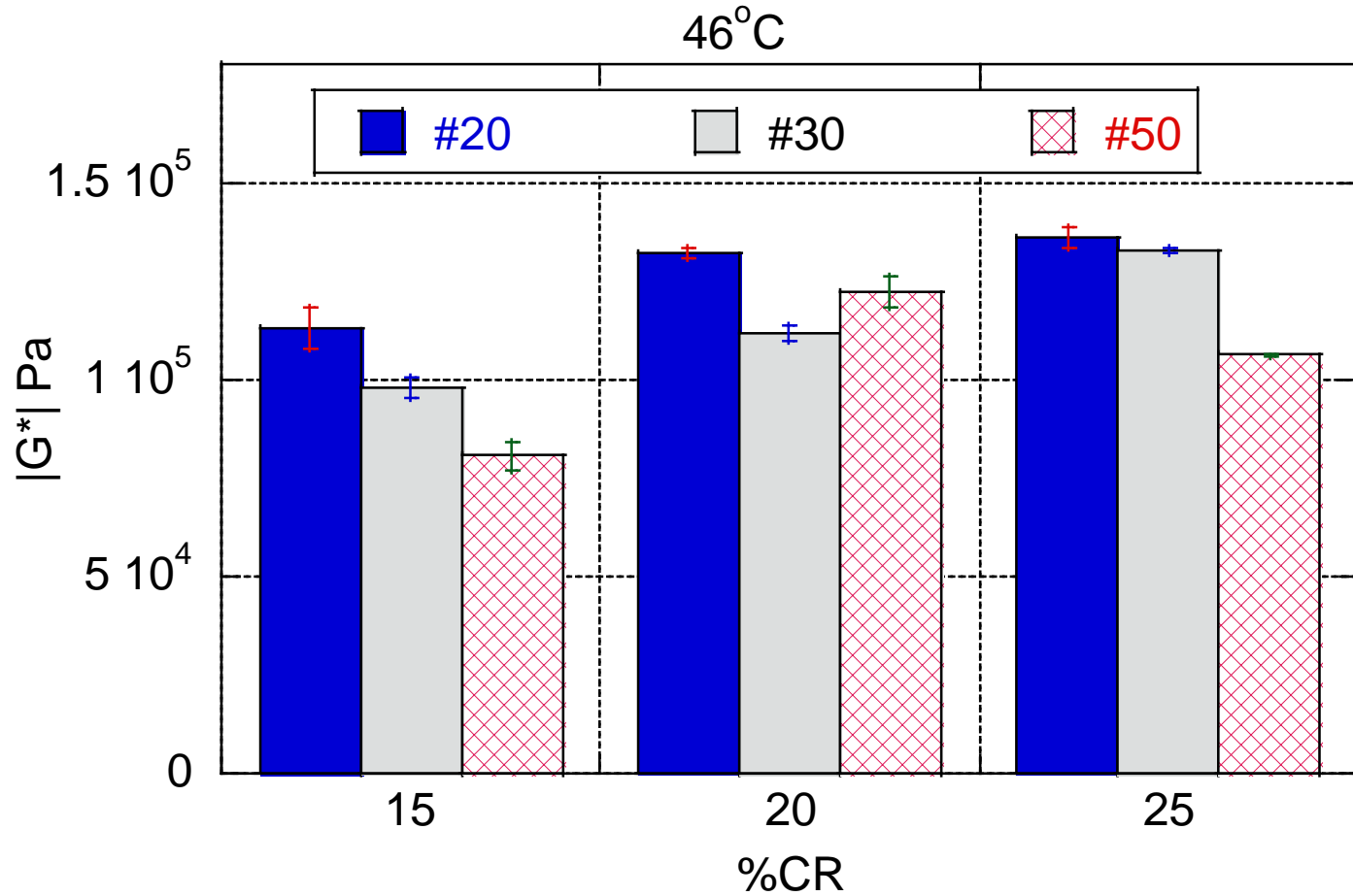
$|G^*|$ at 10Hz



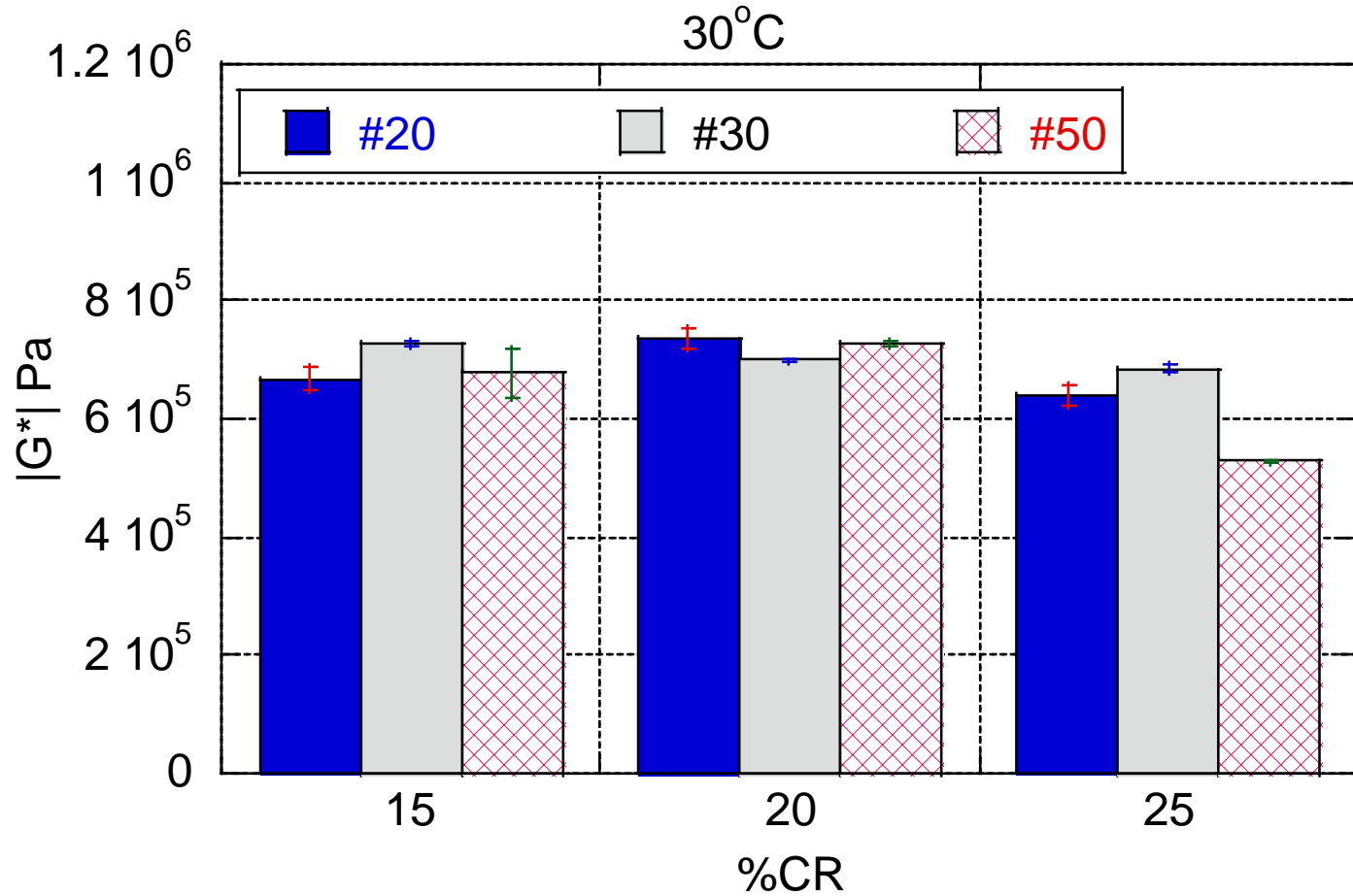
$|G^*|$ at 10Hz



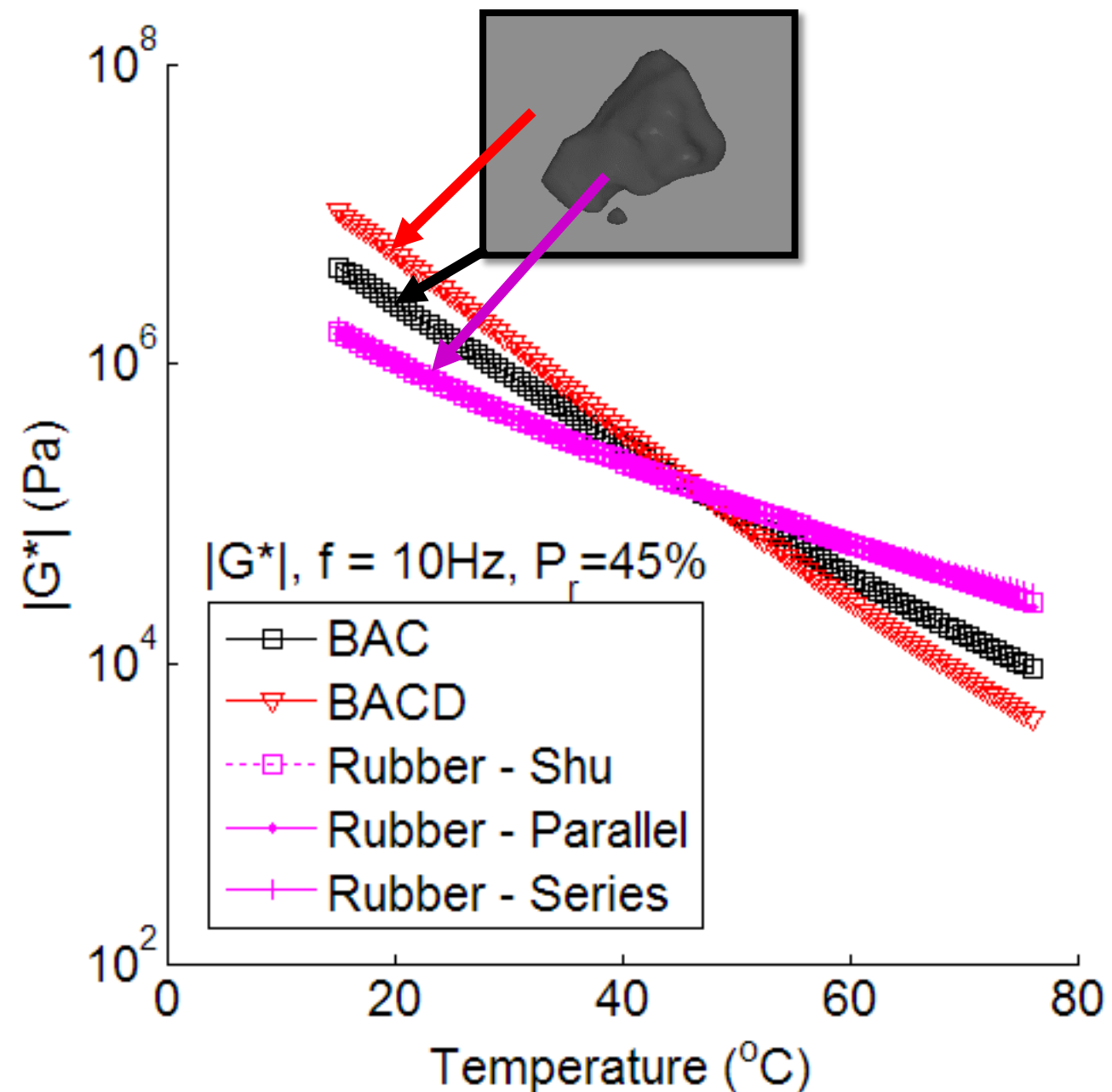
$|G^*|$ at 10Hz



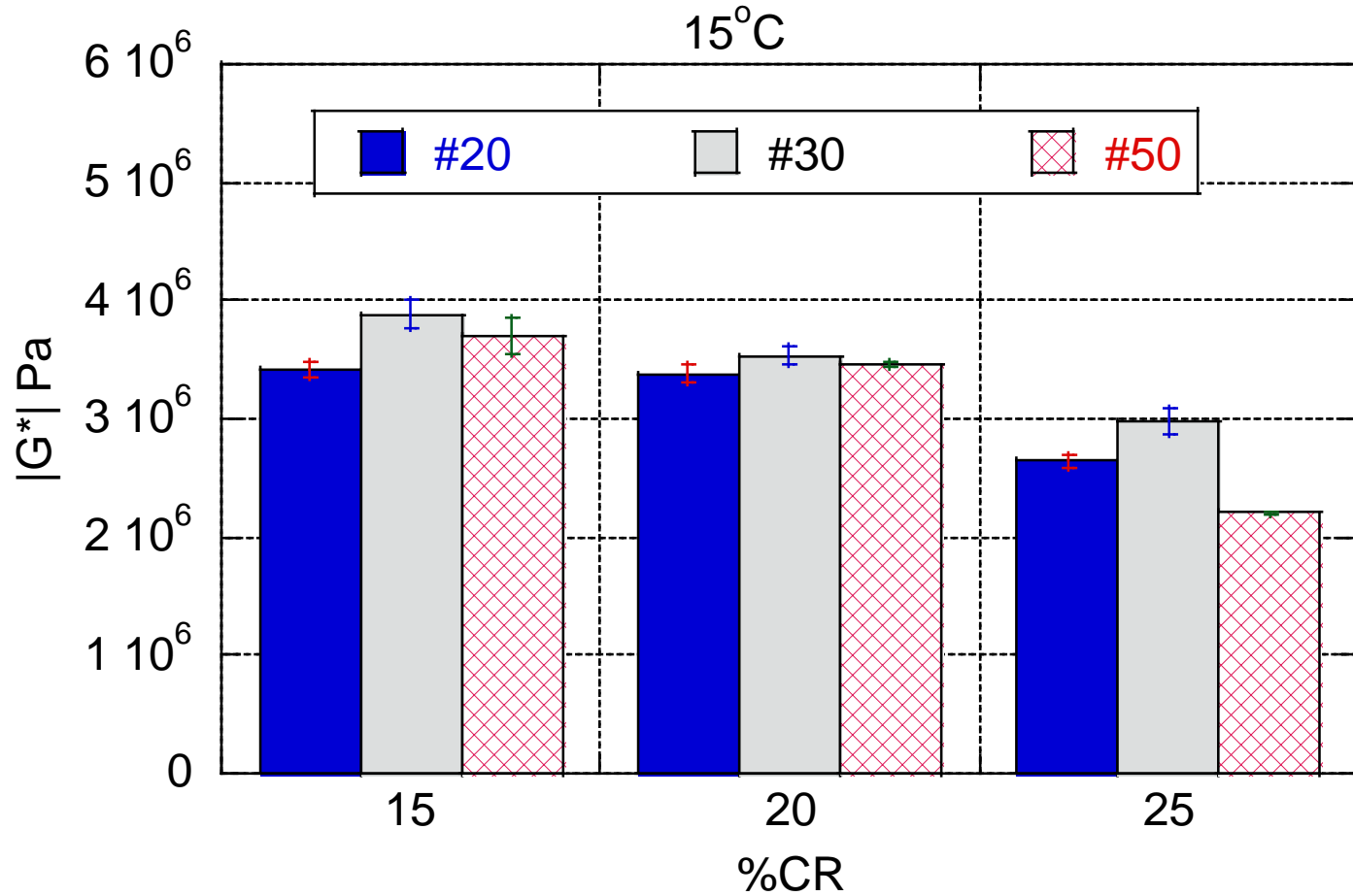
$|G^*|$ at 10Hz



Estimated $|G^*|$ of swollen rubber



$|G^*|$ at 10Hz

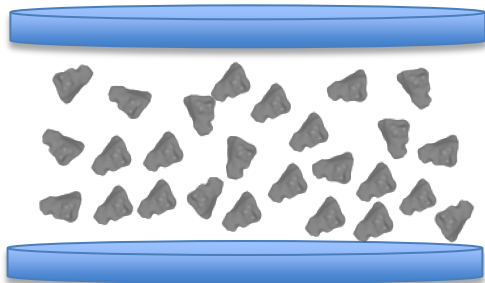


Observations/Conclusions

- At **low CR%** and high DSR temperatures:
 - Significant effect of CR size
 - At **low CR%**:
 - Particle interaction (cushioning) effect becomes visible with increasing CR size

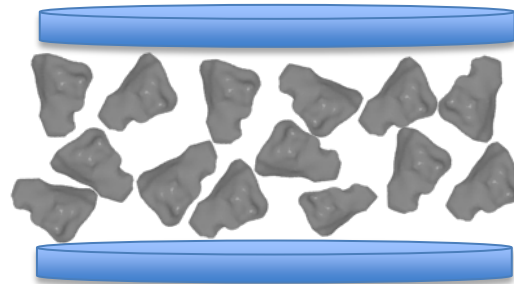
#40-#50

(0.425 – 0.355 mm)



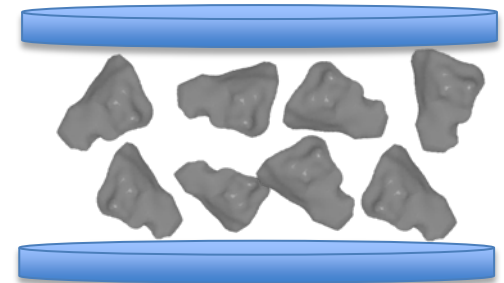
#20 - #30

(0.85 – 0.6 mm)



#16-#20

(1.18 - 0.85 mm)



- At **high CR%** and **low DSR temperatures**:
 - No effect of CR size
 - At **high CR%**
 - Regardless of the CR size, the particles are already interconnected (i.e., cushioned)
- At **low DSR temperatures**
 - Binder between the CR particles are as stiff or stiffer than the CR, therefore, no effect is visible
 - » Material acts like a 'mixture'

- Mixture $|E^*|$ versus $|G^*|$
 - Is it more appropriate to intentionally test the “rubber” in DSR?
 - Rubber modified binder is already “squeezed” between the aggregates
 - Does running the CR binder tests in “loose state” more or less representative of behavior in mixture.
- Repeat the tests using concentric cylinder
 - Compare with mix $|E^*|$

THE END